DopplerScatt Instrument Concept for Simultaneous Measurements of Ocean Surface Vector Winds and Currents - Spaceborne Architecture and Airborne Instrument Test Results

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Why Measure Ocean Currents?

0.72

0.64

0.56

0.48

0.40

0.24

0.16



Image of modeled ocean surface currents from the high resolution ECCO2 model.

Currently, we have no way to validate these results at high resolution.

~2400km

- Ocean surface currents are an essential climate variable
- Knowledge of ocean surface currents will improve our knowledge of energy transfer between the atmosphere and the ocean and our understanding of the advection of heat, nutrients, and pollutants in the ocean.
- Ocean surface currents are a unique complement to the geostrophic currents measured by the forthcoming SWOT mission.





- Coherent radars can measure radial velocities by measuring Doppler shifts.
- The use of Doppler for one component of the surface current velocity has been demonstrated from space using SAR's.
 - Since SAR only looks in one direction, only one component of the velocity is retrieved.
 - Swath width and data rate limitations make SAR's impractical for global coverage
- Rodríguez (2012, 2014) has extended the concept to be able to measure *both* components by using a pencil-beam scanning scatterometer.
 - A wide swath coverage would enable global coverage in one day
 - The same instrument would also measure high resolution winds
- The DopplerScatt IIP will demonstrate the feasibility and accuracy of this concept using an airborne instrument and the results will be applicable to future spaceborne missions.



Comparison of surface current radial component measured by ASAR and geostrophic currents from the AVISO altimetry product. Rouault, M. J., Mouche, A., Collard, F., Johannessen, J. A. & Chapron, B. Mapping the Agulhas Current from space: An assessment of ASAR surface current velocities. Journal of Geophysical Research 115, (2010).





Spaceborne Instrument Concept



Earth Science Technology Office



Space-borne Concept Doppler and Range Coordinates







2 Ka-band beams

- Separated in frequency and incidence angles
- Burst-interleaved: 2 bursts in flight
- Beams: pulse-interleaved
- Slice processing
- **Cell aggregation**

Orbit (sun-synchronous)

- 705 km Altitude:
- Inclination: 98.14 deg
- Velocity: 7560 m/s

Ka-band configuration:

- Look angle: 45.72 and 46.18 deg Incidence: 52.66 and 53.25 deg Frequency: 35.75 GHz Pulse width: 65 us 12 ms Burst width: Burst Repetition Interval: 4.3 ms Number of pulses: 8 pairs Rotation rate: 14 rpm Beamwidth: 0.83 x 0.27 deg 0.3 x 5 km Resolution: Footprint: 26 x 5 km Slice size: 3.7 x 5 km Cell size: $5 \times 5 \text{ km}$ 1.589 km
 - Swath:





Ka-band Instrument Block Diagram



 Ka Doppler Radar block diagram showing its subsystems (PIA, DES, RFES, antenna and spin mechanism), electrical interfaces and hardware maturity levels.







AIRBORNE RADAR HARDWARE STATUS AND TESTS





Parameter	Value (CBE)
Center Frequency	35.75 GHz
Peak Transmit Power	90 W (110W)
Burst Repetition	8 kHz (4.7 kHz)
System Noise Figure	10 dB (6 dB)
Antenna Rotation Rate	5-25 rpm (12.5 rpm)
Antenna Beamwidth	2.9 deg
Velocity Bias	1.0 cm/s
Velocity Precision	10 cm/s
Wind Speed Accuracy	2 m/s (3-20 m/s) 10 % (20-30 m/s)
Wind Direction Accuracy	20 deg
Resolution cell size	5 km













Mechanical Layout





Completely Integrated DopplerScatt







Bottom View







- Goals of antenna range measurements:
 - Characterize the antenna pattern and its geometric relation to the center of navigation.
 - Verify radome insertion loss vs azimuth angle
 - Identify variations of the radome vs azimuth angle due to material or manufacturing irregularities.



Configuration with Radome



FWD marker

Antenna position during measurements



IMU tray





Radome Positions



Nominal



+45°



+90°



+135°



+180°



+225°



+270°



+315°





Radiation Pattern wrt Azimuth Angle with Radome







16

6/13/16



Previous Results: Phase Comparison



- Pulse-pair phase difference, with Pulse 1 (beginning of the burst) as a reference. Nominally, this should be 0 deg.
- In SSPA case, there is progressively larger phase difference, as the pulse separation within the burst increases. Effect seems more pronounced at low temperatures, less at room or hotter temperatures.
- No such effect visible in No SSPA case.





Delay line, temperature control set to 26°C, then off after 1h



100 100 100 100 90 90 90 90 Phase (deg) 80 80 80 80 70 70 70 70 60 60 60 60 50 L 50 L 50 L 50 L 0 100 200 300 400 500 0 100 200 300 400 500 0 100 200 300 400 500 100 200 300 400 500 0 Pulse #4 Pulse #5 Pulse #6 Pulse #7 110 110 110 110 100 100 100 100 90 90 90 90 Phase (deg) 80 80 80 80 70 70 70 70 60 60 60 60 50 ∟____ −100 50 L 50 -100 50 L 0 100 200 300 400 500 0 100 200 300 400 500 0 100 200 300 400 500 0 100 200 300 400 500 Pulse #8 Pulse #9 Pulse #10 Pulse #11 200 200 200 200 150 150 150 150 100 100 100 100 50 50 50 (deg) 50 0 0 Phase -50 -50 -50 -50 M mm -100 M M -100 -100 -100 -150 -150 -150 -150 -200 L -100 100 200 300 400 500 -200 -100 300 400 500 -200 -200 L 300 400 500 300 400 500 0 0 100 200 100 200 0 100 200 0 Pulse #12 Pulse #13 Pulse #14 Pulse #15 200 200 200 200 150 150 150 150 100 100 100 100 50 50 50 50 Phase (deg) 0 0 0 -50 -50 -50 -50 MMM, M M -100 www -100 -100 -100 -150 -150 -150 -150 -200 L 0⁻²⁰⁰-100 0 100 200 300 400 500 -100 0 100 200 300 400 500 100 200 300 400 500 100 200 300 400 500 0 0 Time (min) Time (min) Time (min) Time (min)



Pulse #3

110

/u/vayu-r0/galtamas/plots/20160404_085805/20160404_085805_SOCP_0000.L1A.nc.wavg.dat Phase of the peak for each pulse over time

110

Pulse #2

Pulse #1

110

Pulse #0



Delay line, temperature control set to 26°C, then off after 1h



/u/vayu-r0/galtamas/plots/20160404_085805/20160404_085805_SOCP_0000.L1A.nc.wavg.dat Difference between Cal and Return pulse phase diffs





DopplerScatt Coverage/Verification experiment





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Data SIO, NOAA, U.S. Navy, NGA, GEBCO Image Landsat Data LDEO-Columbia, NSF, NOAA



DopplerScatt from space

- Spaceborne DopplerScatt architecture has been defined as well as key driving requirements
- The TRLs of available technologies for space have been assessed and the Kaband frequency has been chosen with the requirement on the peak transmit power of 100-200W for a fully spinning radar system.

Airborne DopplerScatt progress

- System is fully integrated into its flight configuration
- System post-processing calibration of SSPA behavior has been identified as one of the key efforts
- DopplerScatt has been tested end-to-end through the Optical Delay Line
- It has been integrated with the RSL's King Air B200 in the existing nadir port
- The engineering flights are on-going

