Infrared Correlation Radiometer
for GEO-CAPE
Earth Science Technology Forum 2010

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Measurement of tropospheric CO from space requires a technique capable of high effective spectral resolution and high signal-to-noise.

Correlation radiometry excels in providing both.

Correlation Radiometer Terra/MOPITT has delivered 10 years of the global distribution and seasonal variability of CO in the mid-troposphere measured in MWIR (4.7 um).

Combining MWIR and SWIR (2.3 um) CO from space achieves vertical resolution as required by Decadal Survey.

MOPITT team estimates a factor of 5 more instrument noise in SWIR than in MWIR measurements.

This IIP addresses the signal to noise challenges for 2.3 um measurements for CO.
Objective

• Characterize the noise and spectral performance of a laboratory prototype of the SWIR (2.3 mm) subsystem of an infrared gas filter correlation radiometer for geostationary carbon monoxide (CO) measurements.

• Verify the analytical instrument model to guide evolving GEO-CAPE mission implementation decisions.

Measurements at both 2.3 µm and 4.6 µm are required to obtain lower tropospheric CO. The Decadal Survey’s focus on the lower troposphere placed emphasis on the 2.3 µm measurements.

Approach:

• Design and fabricate the 2.3 µm subsystem of an infrared gas filter correlation radiometer specifically tailored for geostationary measurements.

• Characterize performance to quantify instrument response functions (spectral, spatial, radiometric, and polarization), and explicitly, an end-to-end noise performance characterization.

• Incorporate these characterizations into the CO measurement modeling system for use in GEO-CAPE mission formulation and payload system engineering.

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Key Milestones *

• Internal design and cost 08/08
• Contracts in place 02/09
• System Requirements Review 06/09
• Critical Design review 11/09
• Test Plan Review 04/10
• Breadboard Assembly complete 09/10
• Characterizations complete 11/10
• Instrument Performance Model complete 01/11
• IRCRg Final report 01/11

Breadboard Hardware TRL\textsubscript{in} 3 \rightarrow TRL\textsubscript{now} 4 \rightarrow TRL\textsubscript{out} 5-6
Instrument Model TRL\textsubscript{in} 3 \rightarrow TRL\textsubscript{now} 4 \rightarrow TRL\textsubscript{out} 6
Example Spectral Radiance for different CO Concentrations at 2.3um SWIR lines
IRCRg IIP Project Objectives

To develop a software-based IRCRg instrument performance simulation model that can be used to:

(1) simulate end-to-end IRCRg system performance and CO measurement capability in a “dynamic” environment, and
(2) quantify individual critical IRCRg CO measurement error sources, by the “static” state of the instrument as well as the “dynamic” state of the instrument/host vehicle.

To construct a breadboard laboratory CO IR Gas Correlation Radiometer (IRCRg) instrument that will be used to:

(1) populate the model with actual performance data and, where appropriate, test model performance against laboratory test data.
(2) raise TRLs of critical subsystems of future flight IRCRg instrument for the GEOCAPE mission to provide continental-scale CO mapping from a geosynchronous platform.
Pointing is part of the L1 Requirements for GEO

<table>
<thead>
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<th></th>
<th>Terra</th>
<th>GEO</th>
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<tbody>
<tr>
<td>Altitude, km</td>
<td>705</td>
<td>35,786</td>
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<tr>
<td>Surface size of pixel, km</td>
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<tr>
<td>Pixel viewed angle, degree</td>
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<td>0.0064</td>
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<tr>
<td>Pixel viewed angle, microradians</td>
<td>31,196</td>
<td>112</td>
</tr>
</tbody>
</table>

- The angular size of a GEO-CAPE pixel is 0.0036 of a MOPITT pixel.
- A GEO-CAPE pixel sees an angle smaller than 1 percent of the angle seen by a MOPITT pixel.
- To co-add repeated samples of a pixel, one needs to know which pixels to co-add, therefore one needs to know pointing.
IRCRg Field of View Requirement

- Requirement: Field of view covers US “Lower 48”
- Coverage of the US “Lower 48” requires a 7° horizontal instrument field of view
- Use of a 1024 x 1024 detector array results in:
  - Pixel field of view (IFOV) \(~112\) microradian
  - Pixel foot print \(~4\) km \(\text{center of US}\)
The Simulator: Nuts & Bolts
Modeling Block Diagram

- Terrestrial Atmosphere and surface BDRF Statistics
  - IDL Radiation Transport code
  - Analysis of Statistical & Systematic Errors
- Optical design
- ZEMAX runs
- Orbital Platform Specs
- Sensor Model
- Data Collection Mode
- FPA Testing
- FPA Specs
- FPA Specs
Performance Model: Realistic Instrument Optimization
and Performance Assessment Tools

\[ \begin{align*}
\mathbf{x}, \mathbf{y} & - \text{observation angles} \\
x, y & - \text{image coordinates} \\
\mathbf{X}, \mathbf{Y}, \mathbf{Z} & - \text{latitude, longitude, altitude} \\
A(\mathbf{X}, \mathbf{Y}, \mathbf{Z}) & - \text{Surface albedo} \\
p(\mathbf{X}, \mathbf{Y}, \mathbf{Z}) & - \text{Pressure} \\
T(\mathbf{X}, \mathbf{Y}, \mathbf{Z}) & - \text{Temperature} \\
c_i(\mathbf{X}, \mathbf{Y}, \mathbf{Z}) & - \text{Mixing ratio of species } i \\
r_{sat}, t & - \text{Observer Coordinates} \\
R(\mathbf{X}, \mathbf{Y}) & - \text{Radiance} \\
C(x, y) & - \text{Instrument counts} \\
\mathbf{X}^2 C & - \text{Covariance of instrument counts} \\
\end{align*} \]
Sensor Model Inputs

Each run of the sensor model C code takes an input hypercube (binary file) and a range of sensor parameters, specified in a text file, but shown is a list of considered parameters

- Radiance model output (high spatial res, 500m GSD input)
- Orbital Parameters
  - range, viewing angle, etc
- Optical Parameters
  - focal length, Zernike polynomials, transmission, stray light
- FPA Characteristics
  - noises, per pixel gain/offset curves, hot/cold pixels, array dimensions, crosstalk, well capacity, ADC non-linearity, residual charge
- Platform Characteristics
  - Attitude Control Parameters
- General Parameters
  - Frames to compute, input and output filenames, seeds for PRNGs
Sensor Model

Hi-Res Hypercube Radiance Model

- Background (W/m²/nm/sr)
- IFOV² (sr)
- Dark Current (e/sec/pixel)
- Autoregressive model
- Optical Model
- Jitter Model
- System Transmission (percent)
- Quantum Efficiency (percent)
- T_i (int time) (sec)
- Autoregressive Jitter Model
- Integrate over sub-integrations
- W/nm/pixel
- / hχ (photons/J)
- DC Bias Correction
- Poisson
- Read noise: \( \sigma_r^2 = \text{const} \)
- Shot noise: \( \sigma_{\text{sig}} = G \sqrt{y} \)
- Add read and shot noise
- Non-linear readout
- Quantize (floor)
- Quantize (floor)
- DONE
- Warning
- assuming no spill-over
- min(e/pixel, well depth)
- \( (T_i + T_{\Delta}) \sim \text{full int time} \) (sec)
- e/pixel
- e/sec/pixel
- counts/pixel
- shots/nm/sec/pixel
- photons/nm/sec/pixel
- e/pixel
- e/pixel
- e/sec/pixel
- counts/pixel
Program Flow

Subdivide given integration time and determine instantaneous pointing

Sample hi-res background data after shifting for jitter

Compute optical path difference to get point spread function for this ray

Use PSF to spread the flux for this (x,y) ray onto the focal plane as # of photoelectrons

Repeat process until all rays and all sub-integration times are complete, then loop advance to the next filter position/frame.

Once all looping is complete, add in the dark current, shot noise, read-out-noise, well depth, ADC gain curves, detector non-uniformities, and record in file.
List of Possible Sources of Measurement Sensitivities Currently in the Model

• The sensor model currently incorporates the following:
  – Shot noise from photon statistics (courtesy S.D. Poisson)
  – Scene gradient statistics (from MODIS data @ 2um)
  – Read-out noise from FPA (from testing)
  – Detector dark current, non-uniformity factors, normal/hot/cold pixels, crosstalk, ADC non-linearity, residual charge (from testing)
  – Jitter from orbital platform (from nominal satellite specifications)
  – Optical imperfections (from ZEMAX model)
  – Thermal expansion (from joint run of ZEMAX and CAD models)
Dynamic Process Modeling

• 3 PRNG Seeds
  – Jitter, Noises, Detector Non-Uniformity
  – Allow rerunning cases again using the “same” random noise

• Autoregressive models used:
  – Estimate future values from previous output

• See paper for a thorough description of pointing effects
Status of Sensor Model Simulations

- Graphical user interface has been completed
  - Generates input parameter files through web browser interface

- Simulation of sensor output frames in digital numbers (DN)
  - Written as a MPI parallelized C code
  - Takes output of radiance code, integrates all other pertinent parameters and turns into digital images
  - Utilizes optical design (aberrations), satellite stability (attitude control model), and nominal focal plane array characteristics

- Matlab code to do basic statistical retrieval of CO concentration using only N$_2$O and CO$_{400}$ filter positions (CH4 not needed as we have not varied CH4 levels yet)

- Completed Work
  - Started determining the trade-space between:
    - Well depth and fill %
    - Readout noise
    - Detector offset and gain drift
    - Jitter
The Simulator: Current Verification
Cutaway view of ICRR telescope assembly
• **Measure effective focal length (EFFL)**
  - Via image magnification from measurements in visible wavelengths and extrapolate to target wavelength.

• **Demonstrate focus**
  - Probe the focus position by making systematic measurements of the PSF in visible wavelengths and at target wavelength.

• **Measure transmission (covered in OCF operations)**
  - Probe the system response in the design spectral band-pass and at points outside to demonstrate out-of-band rejection using a spectrophotometer.

• **Measure stray light (covered in OCF operations)**
  - Perform a point source transmittance evaluation.

• **Measure f-number**
  - Exiting beam diameter and EFFL.

• **Determine Zernike coefficients**
  - Interferometry.
Demonstrating focus in the vacuum chamber is accomplished using the design focal plane. Once the LUPI and collimator alignment is established, a mirror and target wavelength source is introduced to the beam.

- A pinhole (100-µm) is located at the focus which is rigidly connected to the LUPI.
IRCR Incubator – Detector System

- Teledyne H2RG - HgCdTe tailored cutoff 2.5 um for stable 2.3 um response
- Teledyne H2RG HgCdTe detector for 4.6 um response also available
- H2RG is 2K*2K, 32-channel readout. 1K*1K also available
- SIDECAr ASIC board is mounted next to the H2RG in cryogenic environment
  - 36 channels of pre-amps, 16-bit ADCs
  - Outputs data to computer via JADE2 board and USB
Detector Testing – System Noise, Linearity, and Latency

Test noise performance of the combined detector (ROIC) and A/D converter (SIDECAR) system
- Cover readout mode(s) and temperatures not tested by manufacturer or in the literature

Test response of detector over a range of illumination levels
- Test at the flux levels higher than those measured by manufacturer or in the literature

Test temporal response of detector to removal of irradiance
- Test with shorter recovery time than manufacturer
Detector Test Block Diagram

- Blackbody Source
- Shutter (latency test only)
- Reference Detector
- LakeShore Temperature Controller
- USB
- RS-232
- Dewar
- Sapphire Beamsplitter
- Bandpass Filter
- FPA
- SIDECAR ASIC
- LVDS Feedthrough
- JADE2
- USB
- PC
- IDL
- USB
Purpose of End to End Testing

- Determine accurate instrument parameters for use as input into model
- Validate model predictions against hardware testing
  - Use external CO/CH4 cells of known concentration to simulate atmosphere
  - Simulate surface gradients to validate effects of sensor jitter on CO retrieval
End to End Testing
Summary

- Develop a simulator model for a correlation radiometer in the 2.3um band to perform tropospheric CO measurements that includes dynamic effects of the platform

- Current Status
  - On target to finish the IIP first of the year (Jan 2011)
  - End to End testing scheduled to begin in October
  - Simulator currently under use to determine sensitivity to input parameters