ESTC 2008 - ACTIVE OPTICAL SESSION FIBER-BASED LASER TRANSMITTER AND LASER SPECTROSCOPY OF THE OXYGEN A-BAND FOR REMOTE DETECTION OF ATMOSPHERIC PRESSURE

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MOTIVATION



Active Sensing of CO₂ Emissions over Nights, Days, and Seasons (ASCENDS) Launch: 2013-2016 Mission Size: Medium



CO₂ measurements: Day/night, all seasons, all latitudes



Inventory of global CO₂ sources and sinks









atmospheric CO₂ Identification of human-generated CO₂ sources and sinks to enable

effective carbon

trading

Improved climate models and

predictions of

Closes the carbon budget for improved policy and prediction

Simulated Column Mean CO2 (Sep 15, 2002)



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HIGH FIDELITY MEASUREMENTS OF CO₂ ARE REQUIRED TO TRACK SOURCES AND SINKS IN THE GLOBAL CARBON CYCLE

- NASA-GSFC IS WORKING ON A LASER INSTRUMENT DESIGNED TO REMOTELY MEASURE CO₂.
- LARGEST ERROR SOURCES IN THIS MEASUREMENT ARE HUMIDITY AND PRESSURE. PRESSURE REQUIREMENT IS ~2 mbar.
- GLOBAL MEASUREMENTS OF ATMOSPHERIC PRESSURE ARE ALSO APPLICABLE TO WEATHER PREDICTION, ATMOSPHERIC MODELING AND DYNAMIC GRAVITY FIELD MEASUREMENTS: 2008

BACKGROUND



An instrument developed by Korb et al.* demonstrated ~2 mbar accuracy using a differential absorption LIDAR (DIAL) instrument in the oxygen A-Band. Instrument utility was limited by:

LASER TECHNOLOGY (ALEXANDRITE) - DIFFICULT TO FIELD AND INEFFICIENT.

DIAL TECHNIQUE - REQUIRES VERY HIGH LASER POWER FOR SUFFICIENT ATMOSPHERIC BACKSCATTER

THIS RESEARCH ADDRESSES THESE ISSUES BY:

ALTERING THE INSTRUMENT FOR HARD TARGET RETURNS INSTEAD OF ATMOSPHERIC BACKSCATTER

DEVELOPING A LASER TECHNOLOGY TO ADDRESS THE SUBSEQUENT REQUIREMENTS. * APPLIED OPTICS 28 (15), 1989





 $K_R(\tilde{\mathbf{v}}) = n \cdot S_i \cdot f$

LINE SHAPE ANALYSIS



$$T(\tilde{v}) = \exp[-K(\tilde{v}) \cdot L] = \exp\left[-\left(K_c + K_R(\tilde{v})\right)L\right]$$

BEER-LAMBERT LAW WITH SPLIT CONTINUUM AND RESONANT ABSORPTION COEFFICIENTS

- n NUMBER DENSITY S_i - Line strength parameter
- f LINE SHAPE

TEM BRO

GAU

PRE

BRO

(COL LOR



$$\gamma_D = \frac{\tilde{v}_o}{c} \cdot \sqrt{2 \cdot R \cdot \ln(2) \left(\frac{T}{M_{O_2}}\right)}$$

$$f_{L}(\tilde{v}) = \frac{1}{\pi} \cdot \left[\frac{(\gamma_{L}/2)}{(\tilde{v} - \tilde{v}_{o})^{2} + (\gamma_{L}/2)^{2}} \right]$$
$$\gamma_{L}(\tilde{v}_{o}) = \gamma_{air} \cdot P \cdot \left(\frac{T_{o}}{T}\right)^{n_{a}}$$

Temperature
Broadening
(Doppler,
Gaussian)
$$I_{1D}(w)$$

 $fl_D(w)$
 $fl_L(w)$
 $fl_V(w)$ $I_{10}(w)$
 $fl_V(w)$ Pressure
Broadening
(collision,
Lorentzian) $I_{130761-10^6}$ $I_{130762-10^6}$ $I_{130763-10^6}$ $I_{130764-10^6}$ $I_{30765-10^6}$

$$f_V(\tilde{\boldsymbol{v}}) = \int_{-\infty}^{\infty} f_D(\tilde{\boldsymbol{v}} - \tilde{\boldsymbol{v}}_o) \cdot f_L(\tilde{\boldsymbol{v}} - \tilde{\boldsymbol{v}}_o - \boldsymbol{\tau}) d\boldsymbol{\tau}$$

VOIGT - CONVOLUTION OF GAUSSIAN AND LORENTZIAN SHAPES

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η_{Rx}, efficiency of the receiver, includes terms often written out explicitly like area of the receiver telescope, the inverse square dependence on range. These terms have been consolidated for clarity

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LASER REQUIREMENTS SPECTROSCOPY



- **CENTER WAVELENGTH** 760 - 770
- WAVELENGTH TUNABLE ~200 PM
- LASER LINEWIDTH AND STABILITY ~5 MHZ. (REQUIRES >100 NS TRANSFORM LIMITED PULSES)
- SPECTRAL PURITY ~40 DB

REMOTE SENSING

- SINGLE SPATIAL MODE
- HIGH PEAK OPTICAL 1.1 **POWER (HUNDREDS OF** WATTS)



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MEASUREMENT DEMONSTRATION





MEASUREMENT DEMONSTRATING THE CORRELATION BETWEEN PRESSURE AND THE PRESSURE-BROADENED (LORENTZ COMPONENT) LINE-WIDTH

LORENTZ WIDTH WAS CALCULATED USING A LEAST-SQUARES VOIGT FITTING ROUTINE



SBS IS A NONLINEAR INTERACTION BETWEEN A LASER SOURCE AND SOUND WAVES (PHONONS) IN A DIELECTRIC MEDIUM. IT RESULTS IN A LOSS OF POWER IN THE ORIGINAL SIGNAL AND A BACKWARD PROPAGATING STOKES SIGNAL AT A SLIGHTLY INCREASED WAVELENGTH.

SBS CAN APPEAR IN FIBER LASERS AND AMPLIFIERS DUE TO THE COMBINATION OF HIGH OPTICAL POWER, CONSTRAINED SPATIAL MODE AND LONG INTERACTION LENGTH. SBS APPEARS IN FIBER LASERS AND AMPLIFIERS FOR PEAK POWERS AS LOW AS ~10W WHEN OPERATING IN NARROW LINE-WIDTH (<100MHz) AND IN CW OR LONG PULSE MODE.</p>

THE PARASITIC NATURE OF THE SBS SIGNAL DRAINS POWER FROM THE MAIN SIGNAL. IT IS THE PRIMARY NONLINEAR AFFECT LIMITING THE PERFORMANCE OF THE FIBER TRANSMITTER.





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1.2 beam radius [mm] $M^2 = 1.09$ NEAR DIFFRACTION $M^2 = 1.03$ LIMITED BEAM QUALITY DEMONSTRATED IN **BOTH AXES** EXCELLENT POLARIZATION EXTINCTION RATIO 0 (20DB) 50 100 150 200 0 z-position [mm]



FREQUENCY-DOUBLING



- ~265 WATTS (PEAK) OF FUNDAMENTAL PUMP POWER
- 56% CONVERSION EFFICIENCY
- ~150 WATTS OF PEAK OPTICAL POWER AT 770 NM
- <1% DUTY CYCLE





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TEMPERATURE SENSITIVITY



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OPEN PATH TRANSMISSION

MEASUREMENT



440 METER OPEN PATH **MEASUREMENT (SLOW** SCAN ~1HR)

COMPARISON BETWEEN MEASUREMENT AND THEORY CALCULATED WITH PARAMETERS FROM HITRAN AND A COINCIDENT WEATHER

MEASUREMENT TAKEN IN DESIRED SPECTRAL



- FASTER SCANNING ENABLED BY PULSE INTEGRATION ELECTRONICS
- FASTER SCANNING WILL ALLOW BETTER INDIVIDUAL MEASUREMENTS AND MORE AVERAGING
- IMPROVE INSTRUMENT DATA COLLECTION AND PROCESSING
- IMPROVED DATA ANALYSIS SOFTWARE
- MORE SENSITIVE DETECTORS
- SOLAR FILTERS
- LONGER ATMOSPHERIC PATH LENGTH FOR HIGHER ABSORPTIONS
- **DEMONSTRATE ATMOSPHERIC PRESSURE SENSITIVITY**



CONCLUSIONS



- DEMONSTRATED FIBER-BASED LASER TRANSMITTER WITH: NARROW FREQUENCY, WAVELENGTH TUNING, SPECTRAL PURITY, POLARIZED OUTPUT, SINGLE SPATIAL MODE OPERATION, PULSE MODULATION,
- DEMONSTRATED POWER SCALING
- DEMONSTRATED EFFICIENT FREQUENCY-DOUBLING
- DEMONSTRATED OXYGEN A-BAND SPECTROSCOPY
- BUILT INITIAL VERSION OF REMOTE SENSING INSTRUMENT





BACK-UP SLIDES

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- MEASUREMENT OF SEED LASER MADE WITH A 50 PM RESOLUTION OPTICAL SPECTRUM ANALYZER (OSA)
- DFB SEED LASER SHOWS 40 DB OF SIDE BAND SUPPRESSION
- MEASUREMENT MADE WITH A PZT-SCANNED FIBER FABRY-PEROT ETALON
- RED CURVE SHOWS THE CALIBRATION SCALE WITH 3 MHZ SIDE-BANDS
- BLUE CURVE SHOW THAT THE LINE-WIDTH IS NOT BROADENED BY AMPLIFICATION

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SPECTRAL PURITY

MEASUREMENT OF THE SPECTRA OF THE AMPLIFIED LASER SIGNAL SHOWING ~40 DB OF SIDE BAND SUPPRESSION.

- SOME RESIDUAL AMPLIFIED SPONTANEOUS EMISSION (ASE) PEAKED AROUND 1545 NM IS OBSERVED. THIS COULD BE FILTERED IF NECESSARY.
- ADDITIONAL SUPPRESSION WILL RESULT AFTER FREQUENCY-DOUBLING

FREQUENCY-DOUBLING

- 23% EFFICIENCY
- FREQUENCY-DOUBLING WAS ACHIEVED WITH A TEMPERATURE CONTROLLED 30 MM PPKTP CRYSTAL
- CONVERSION EFFICIENCY IS ~1/2 OF THEORETICAL LIMIT (FOR THIS INPUT POWER)
- CONVERSION IS PRIMARILY LIMITED BY POWER AT FUNDAMENTAL WAVELENGTH
- POWER AT FUNDAMENTAL IS LIMITED BY SBS

• TRADES

- A_{eff} vs. single spatial mode behavior
- g_{SBS} vs. host, dopants, fiber geometries, spectral width
- Leff VS. GAIN, PULSE/SPECTRAL WIDTH

COMMON SBS MITIGATION TECHNIQUES

- INCREASE FIBER MODE SIZE
- Leff can be reduced by decreasing the laser pulsewidth and/or broadening the signal linewidth . (Our applications require narrow linewidth [long pulses] so this method will not work)
- DECREASE FIBER LENGTH (INCREASE DOPANT DENSITY TO INCREASE GAIN PER UNIT LENGTH.)
- **PUMP WAVELENGTH AT HIGHEST ABSORPTION TO INCREASE GAIN PER UNIT LENGTH**

FIBER DESIGN

- LARGE MODE AREA FIBER (25 µM DIAMETER)
- DESIGN OPTICAL INDEX PEDESTAL AROUND CORE TO MAINTAIN SINGLE MODE OPERATION WITH LARGE CORE AREA
- COIL FIBER TO INCREASE LOSS IN HIGHER ORDER MODES
- MINIMIZE FIBER LENGTH
 - HIGH DOPANT DENSITY FOR HIGH GAIN PER UNIT LENGTH
 - PUMP AT 977 NM FOR MAXIMUM ABSORPTION PER UNIT LENGTH

SEED SOURCE PERFORMANCE

- SEED SOURCE FOR LOW DUTY CYCLE (<1%) OPERATION
 REQUIRED ADDITIONAL
 AMPLIFIER TO BOOST AVERAGE
 POWER
- SECOND AOM INCREASED EXTINCTION RATIO AND SPECTRAL SIDE BAND SUPPRESSION AND NARROWED THE PULSE WIDTH

SPECTRAL PURITY OF AMPLIFIED SIGNAL

TOTAL AMPLIFIED SIGNAL SHOWS 62 DB OF SIDE BAND SUPPRESSION

INSETS ILLUSTRATE THE EFFICACY OF SECOND AOM IN SUPPRESSING IN-BAND ASE

