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# Development of an Agile Digital Detector for RFI Detection and Mitigation on Spaceborne Radiometers

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## Introduction

- RFI can cause significant errors in science data
  - L- and C-Band soil moisture measurements over land
  - L-, C- and X-band ocean measurements
- High levels of RFI are relatively easy to detect
  - Mitigate using analog parallel subband filter approach
- Low levels of RFI present more difficulty
  - Low integrated energy looks like science signal
  - High-power, short-duration  $\rightarrow$  low integrated energy
  - Many sources (*e.g.* air-traffic control radars) match this profile
- Digital signal processing approach
  - Based on statistical properties of natural emission vs. man-made interference





## **Project Objectives**

### Technical Objectives

- Design, develop and field test candidate RFI mitigation detectors
- Develop RFI mitigation algorithms and characterize their performance
  - Empirical field testing
  - Analytical performance models
- Develop a space qualified candidate point design

### Technology Infusion

- Integrate RFI mitigation detectors with established ground based and airborne microwave radiometers
- Demonstrate capabilities to the science community





## **Progress of Technology Infusion**

### • Spaceflight Opportunities

- SMAP mission (recommended by NRC Earth Science Decadal Survey) has included the ADD subsystem in their baseline design
- IPO NPOESS MIS radiometer design studies include versions of ADD in their trade space

#### National Radio Astronomy Observatory

 Frequency Agile Solar Radiotelesope (FASR) national facility includes ADD RFI detection and mitigation subsystem in its baseline design





## **Project Schedule**

- Year 1 (7/05-6/06)
  - Prototype RFI Detector development
  - Ground based & airborne campaigns
- Year 2 (7/06-6/07)
  - Campaign data analysis
  - Define space flight detector requirements
- Year 3 (7/07-6/08)
  - Advanced detection and mitigation algorithm development
  - Spaceflight detector brassboard development
- Follow On
  - Working with SMAP and MIS Programs





# **Theory of Operation**

- Desired radiometric (science) signals generated by thermal noise
  - Amplitude of electric field has a gaussian (bell-curve) probability density function (PDF)
- RFI is man-made
  - PDFs will often be non-Gaussian
- Exploiting this distinction is the basis of the Agile Digital Detector (ADD)





#### **Thermal Noise Amplitude Probability Distribution**







#### **Outdoor Sky Cal with sinusoidal RFI 8 Subband Probability Density Functions**



•  $T_B = 40$  K plus ~260 K sine wave injected into subband 5





## **RFI Detection Using Higher Order Moments**

• The kurtosis of a random variable, *x*, is defined as

$$k = \frac{\langle (x - \langle x \rangle)^4 \rangle}{\langle (x - \langle x \rangle)^2 \rangle^2}$$

- k=3 for a gaussian distributed r.v., independent of  $\sigma_x^2$ (*i.e.* k=3 for natural thermal noise, independent of brightness temperature)
- The standard deviation of an estimate of k after a finite integration time is

$$\Delta k = \sqrt{\frac{24}{B\tau}}$$

- For prototype radiometer operation (B=3 MHz &  $\tau$ =0.3 s),  $\Delta k = 0.005$
- RFI Detection Flag if  $|k 3| > 3\Delta k$





### **C-Band Field Deployment – with NOAA/ETL PSR**

• Operated on WB-57 over Texas, 25 August 2005







Ruf et al., ADD RFI, ESTC 2008



## **Example of PSR Flight Data Kurtosis and 2<sup>nd</sup> Moment Spectra**



- ch = 50-80 (~6 GHz), intermittent times
  - Strong non-gaussian kurtosis
  - Strong, correlated effect on T<sub>B</sub>
- $ch = 170-180 (\sim 7.5 \text{ GHz}), t = 0-60s$ 
  - Strong non-gaussian kurtosis
  - Not so noticeable effect on  $T_B$

 Kurtosis (left) and 2<sup>nd</sup> moment (below) 5.5-7.5 GHz spectra v. time over Dallas Metro area







## Radiometer Brightness Temperature and Kurtosis Images



- Overflight of Galveston, TX coastline
  - TB image (left) sensitive to both natural and artificial emission (artificial emission, coastline and islands all affect TB)
  - Kurtosis image (right) only sensitive to artificial emission







Ruf et al., ADD RFI, ESTC 2008





#### False Alarm Rate and Probability of Detection of Pulsed Sinusoidal RFI

- For RFI power level at brightness temperature equivalent to 2NEΔT, detection threshold can be set to give:
  - 90% probability of detection
  - 3% false alarm rate
- 0.1% duty cycle case corresponds to ARSR-1 operating mode
- Higher duty cycle reduces detection







#### False Alarm Rate and Probability of Detection of Pulsed Sinusoidal RFI



• Plot comparing the ROC area for the kurtosis algorithm under various data rates schemes and subbands with the matched peak detection algorithm (blue \*) (RFI power = 0.5NEDT)





## **Development of ADD Flight Brassboard**





# **ADD Brassboard Requirements**

- Two Channel, V and H polarization
- Input (from RF front end)
  - 1401.75 to 1425.75 MHz band limited (24MHz BW)
  - (-10 dBm) signal amplitude
- Use ADC to
  - downconvert the RF input
  - Sample at Nyquist rate for subsequent digital filters
- Signal Processing
  - $1^{st}$ ,  $2^{nd}$ ,  $3^{rd}$ , and  $4^{th}$  moments for V and H (full BW) and each of 16 subbands
  - 16 equally spaced subband filters (24MHz/16 = 1.5MHz each)
  - Complex correlation of full BW and each of 16 subbands:
    - Real <Iv\*Ih> + <Qv\*Qh>
    - Imag  $\langle Iv*Qh \rangle \langle Qv*Ih \rangle$





# **ADD Brassboard Objectives**

- Purpose
  - Test and characterize ADC and FPGA digital signal processing.
    - System SNR, with analog radiometer data as benchmark
    - Power requirements
    - Mass and physical configuration estimates.
  - Establish requirements
    - ADC clock rate
    - ADC clock jitter specification
    - Power regulation and noise limits, for ADC in particular.
- Design
  - Brassboard parts to be functionally equivalent to space qualified parts.
  - Circuit board layout is critical at high frequency. Successful layout to be duplicated in flight design.





### **Brassboard Block Diagram**







# Conclusions

- Direct measurement of higher order moments (1<sup>st</sup>, 2<sup>nd</sup>, 3<sup>rd</sup> and 4<sup>th</sup>) can be used to reliably detect non-gaussian RFI
- The signal kurtosis is a very robust statistic on which to base a detection algorithm
- Digital subbanding allows RFI to be removed
- Experimental verification demonstrates performance in a relevant science application environment
- In design trade space for two pending spaceborne radiometer programs
- Flight brassboard testing planned for Summer 2008



