

A Ka-band to baseband RF Testbed for the SWOT mission

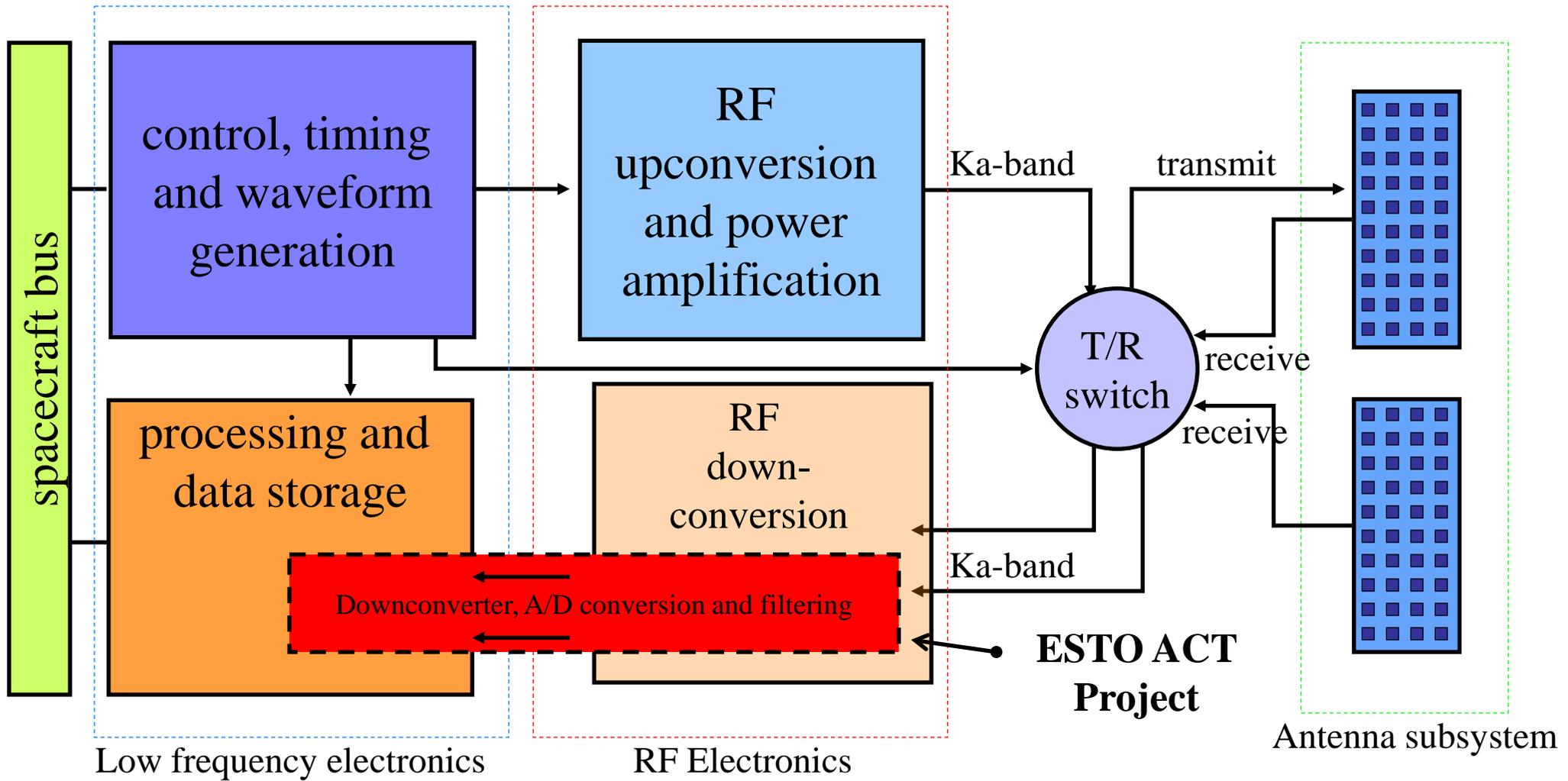
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Fernandez (JPL)

Vishwas Vijayendra, Kan Fu, Tony Swochak,
Tom Hartley (UMass)
Mike Nakashima (JPL)

SWOT RF Testbed

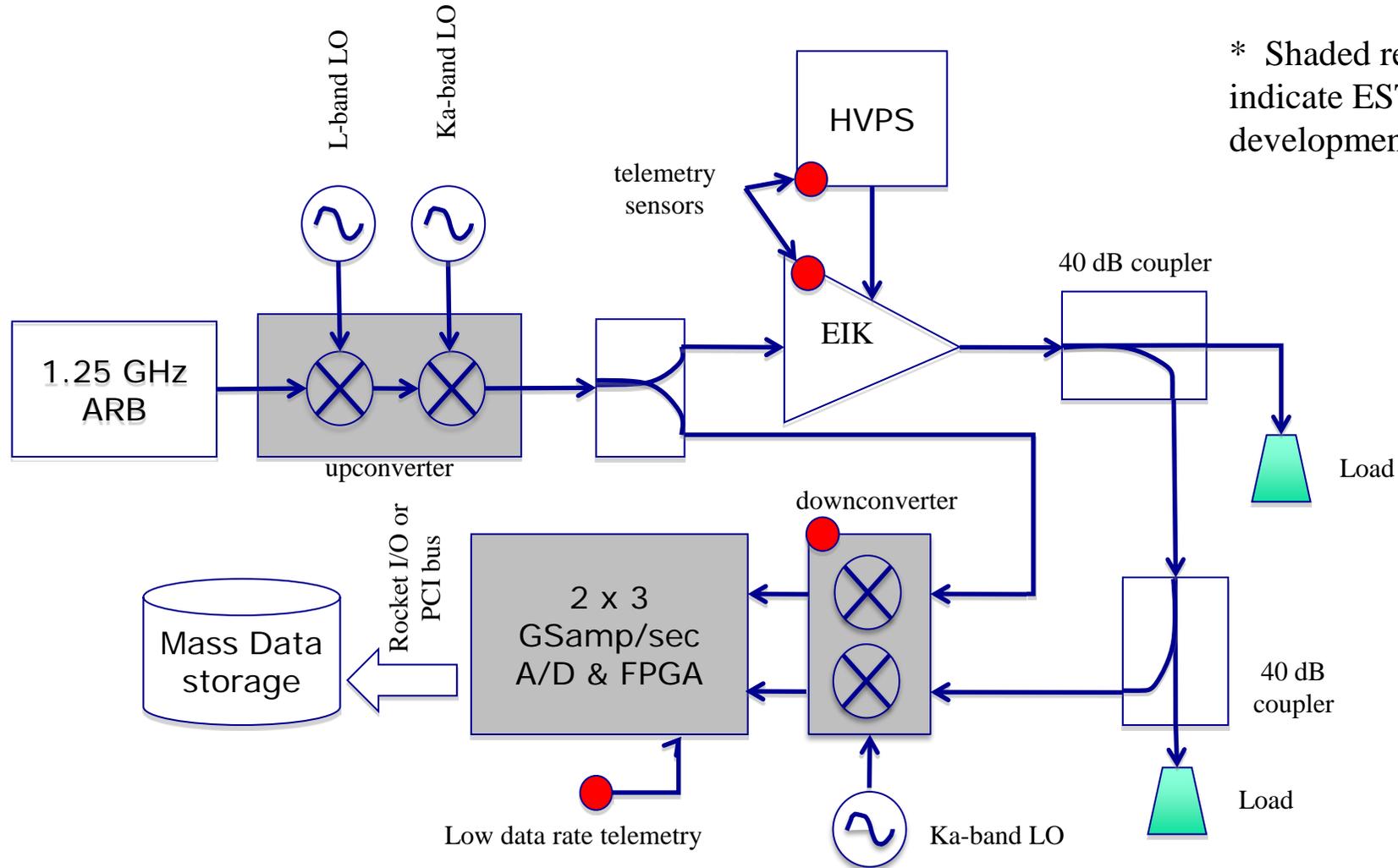
- Based on ESTO funded downconverter development to explore receiver topologies and to characterize/compensate for thermal effects
- Additional testbed parts constructed from available test equipment and RF parts
- Ability to perform tests over temperature
- High-speed (2x3GSamp/sec ADC/FPGA Board) for capturing and processing data in real time
- TRL Advancement

Spacecraft block diagram

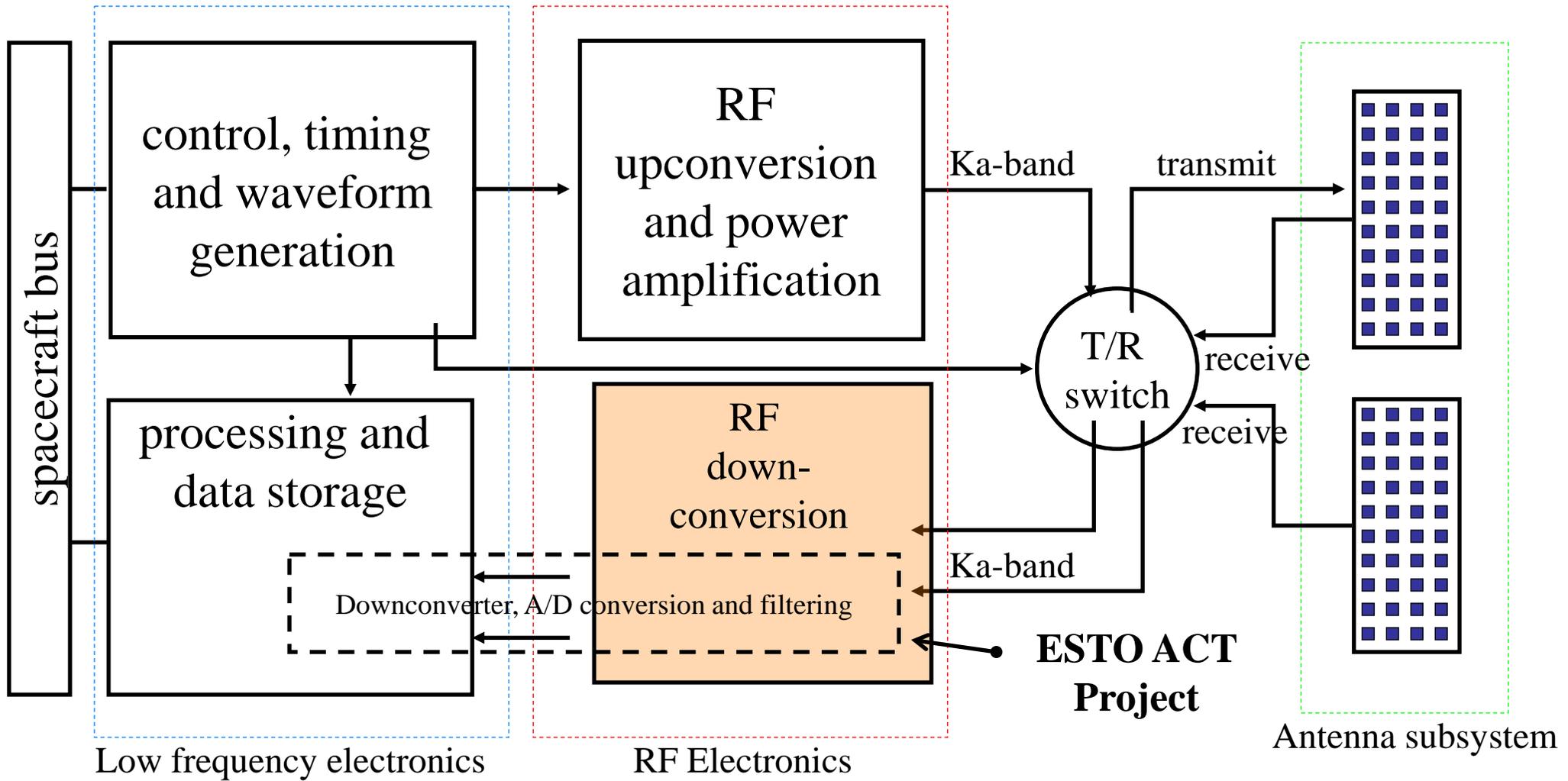


Block Diagram of RF Testbed

* Shaded regions indicate ESTO funded development components

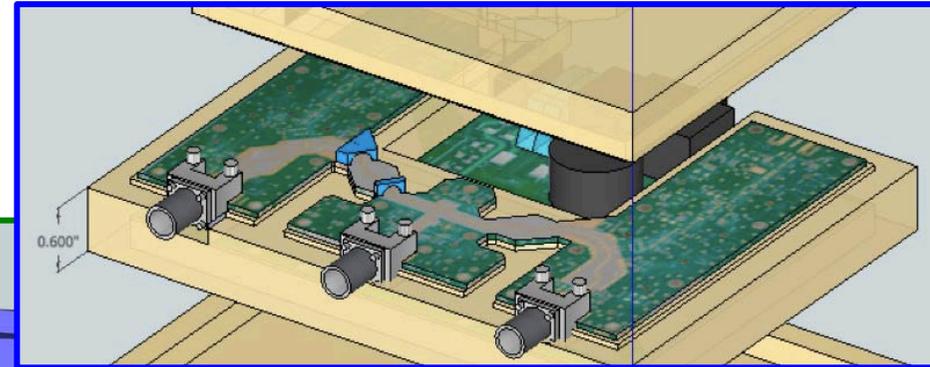
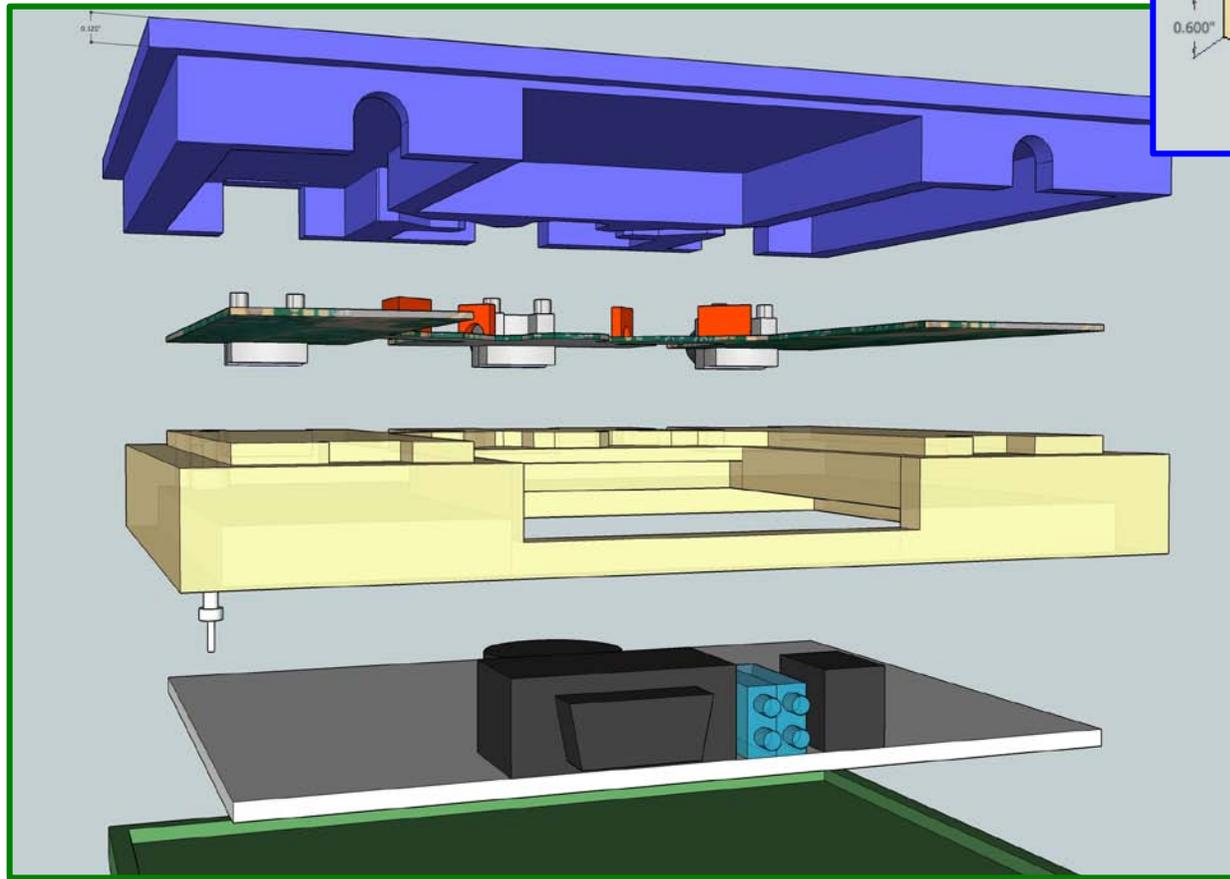


Spacecraft block diagram



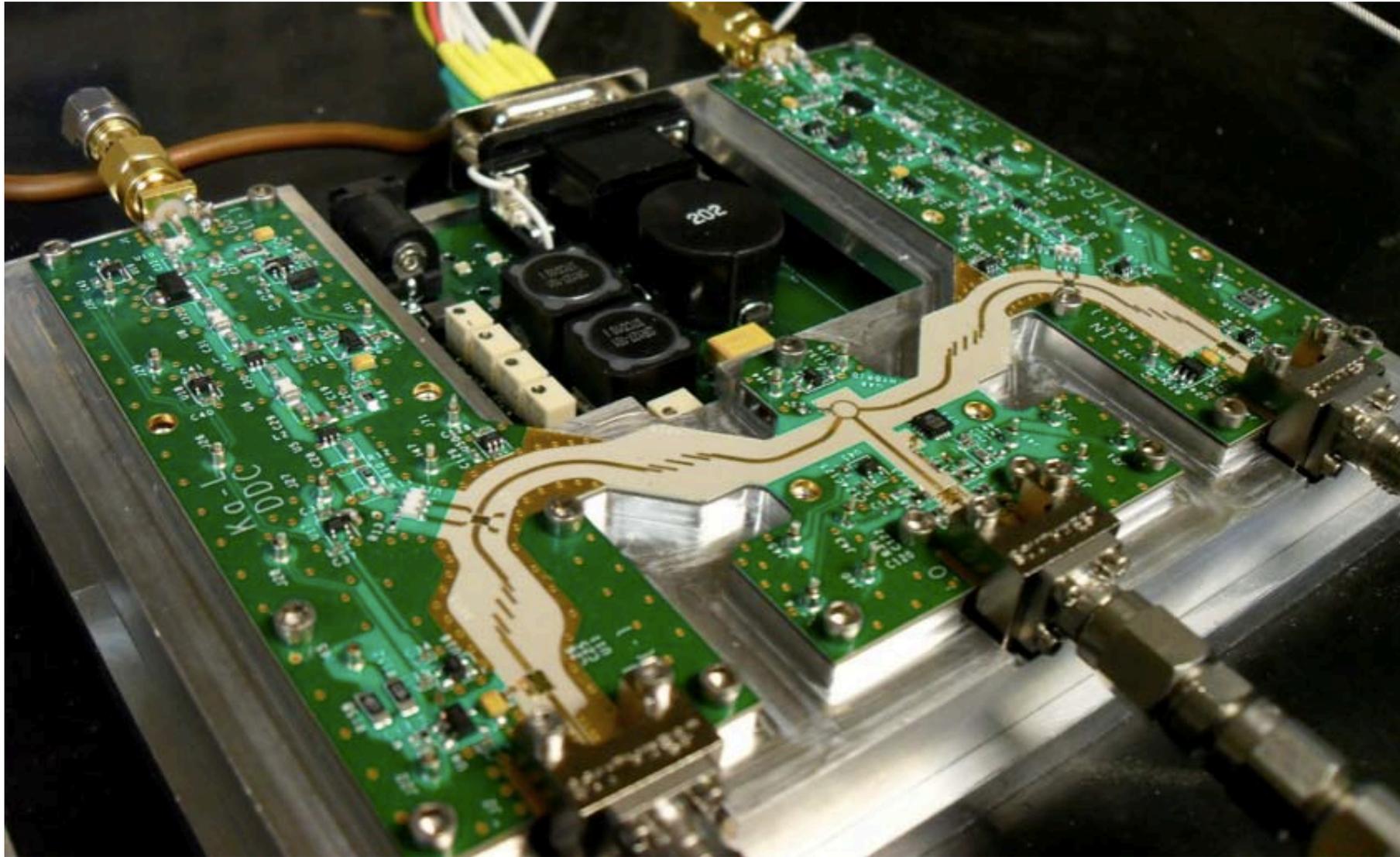
Ka-band downconverter development

SWOT prototype receiver



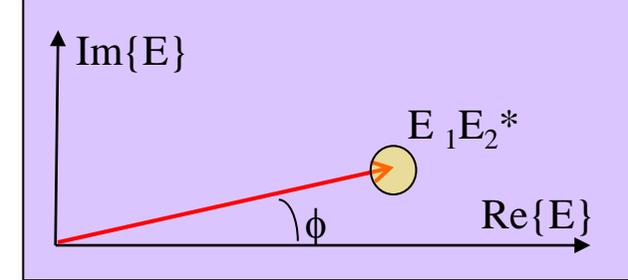
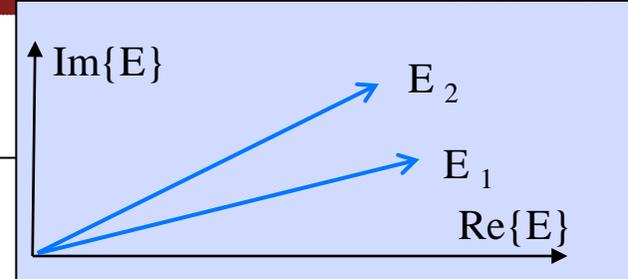
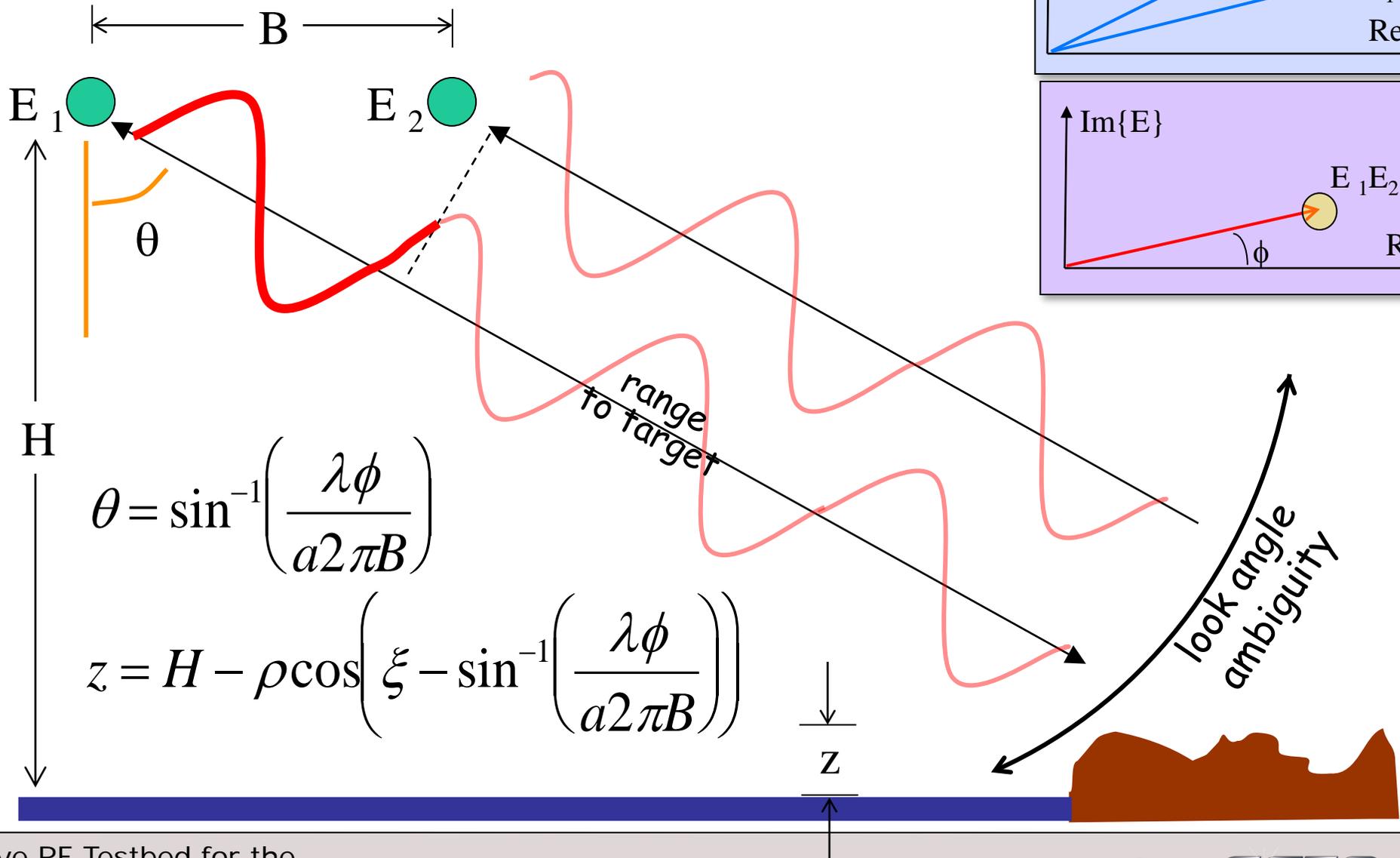
- To improve isolation and thermal management, DC electronics were moved into a secondary cavity
- drop-down walls isolate filter cavities
- between-board connections made with Tusonix through-connectors.
- L-band signal amplified to be directly sampled by A/D converter

Exposed RF subsection undergoing testing

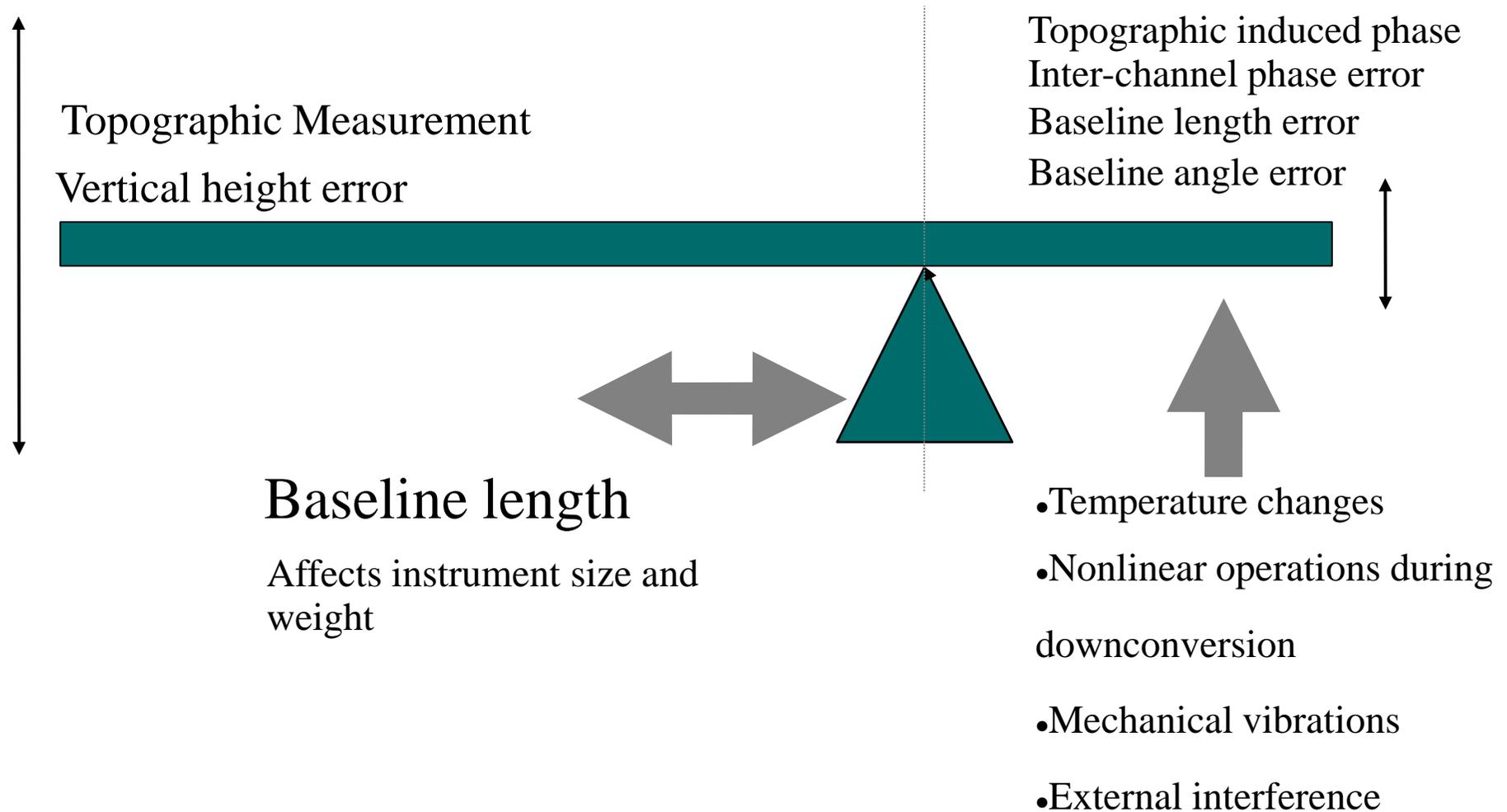


Active RF Testbed for the SWOT Mission

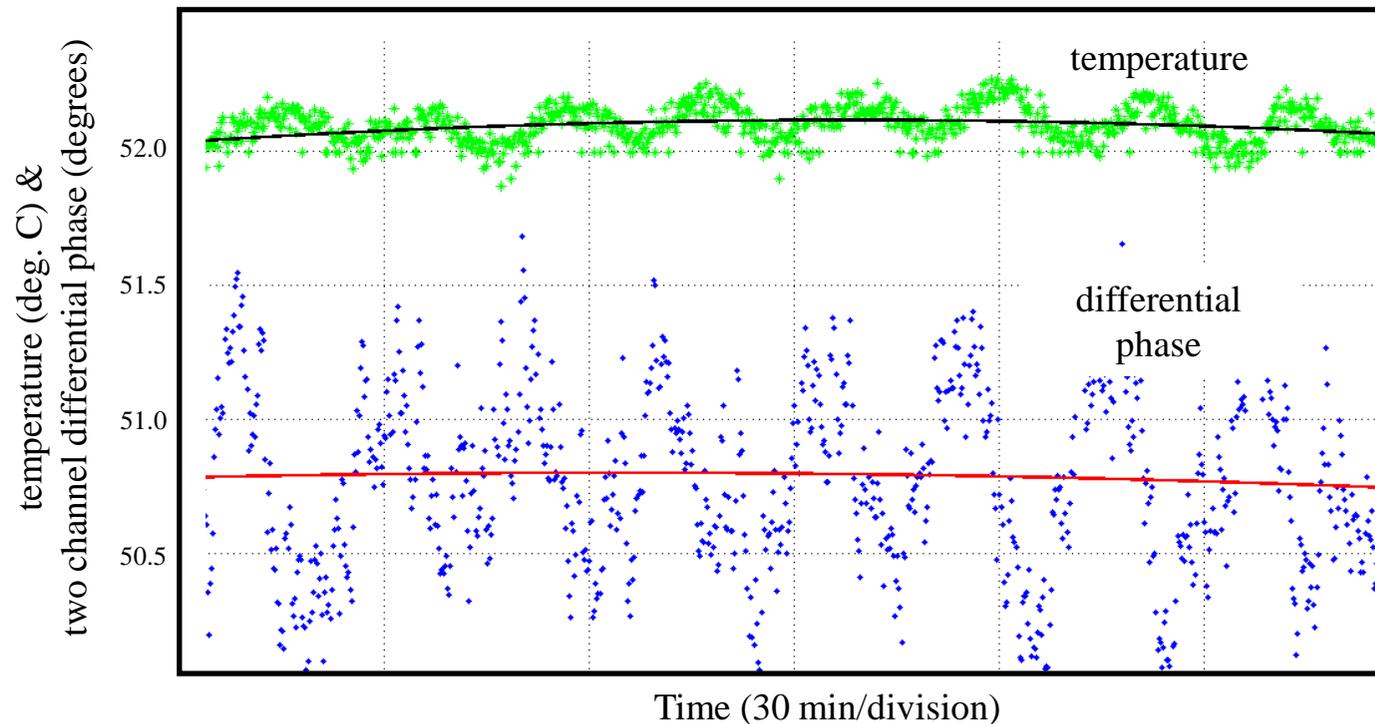
Cross-Track Interferometry



Engineering Challenge



Temperature dependence of differential phase

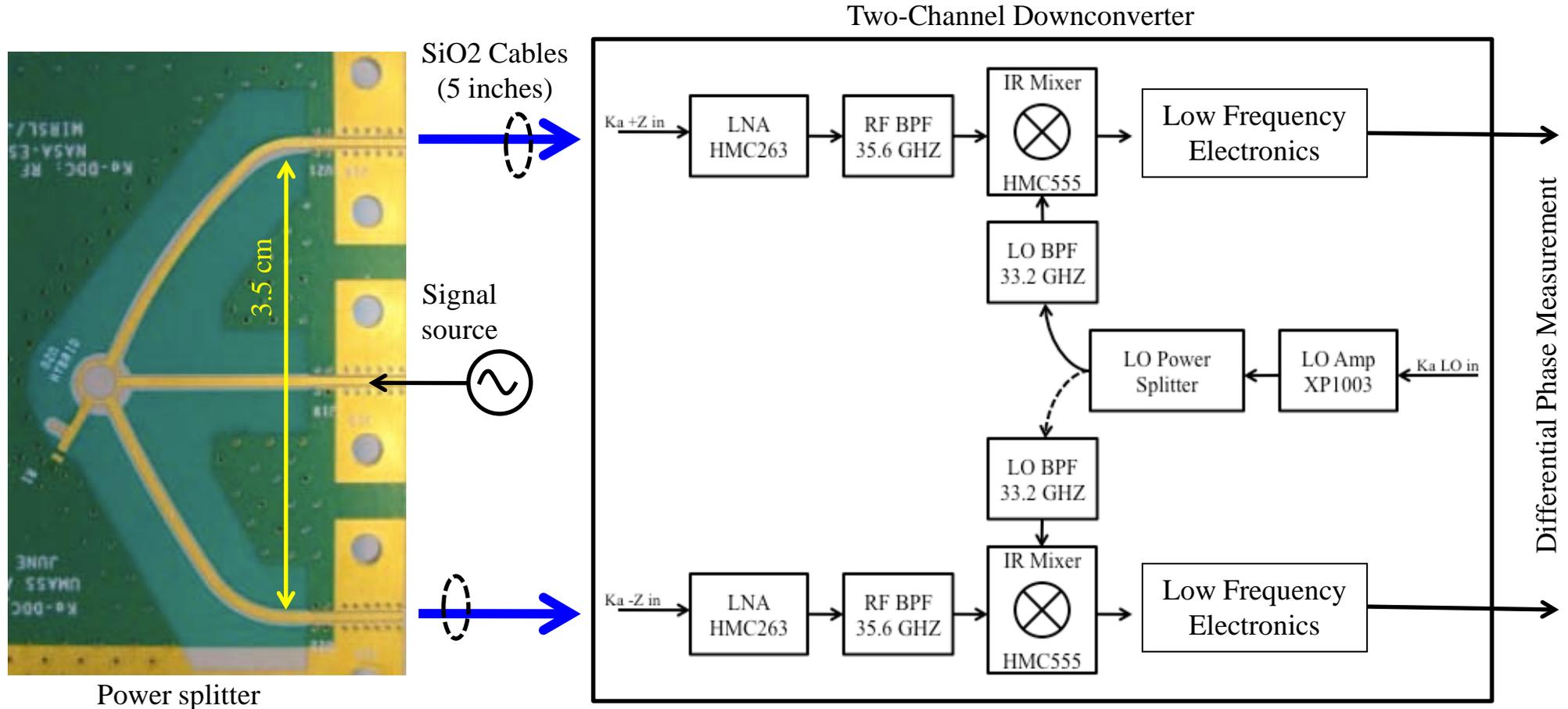


- Concurrent measurements of temperature and differential phase showed a strong dependence of phase on temperature.
- Temperature fluctuations due to the ambient environment. Measurements in a closed environment were much more stable
- Solid lines in the plot indicate a 3rd order polynomial fit to the data.

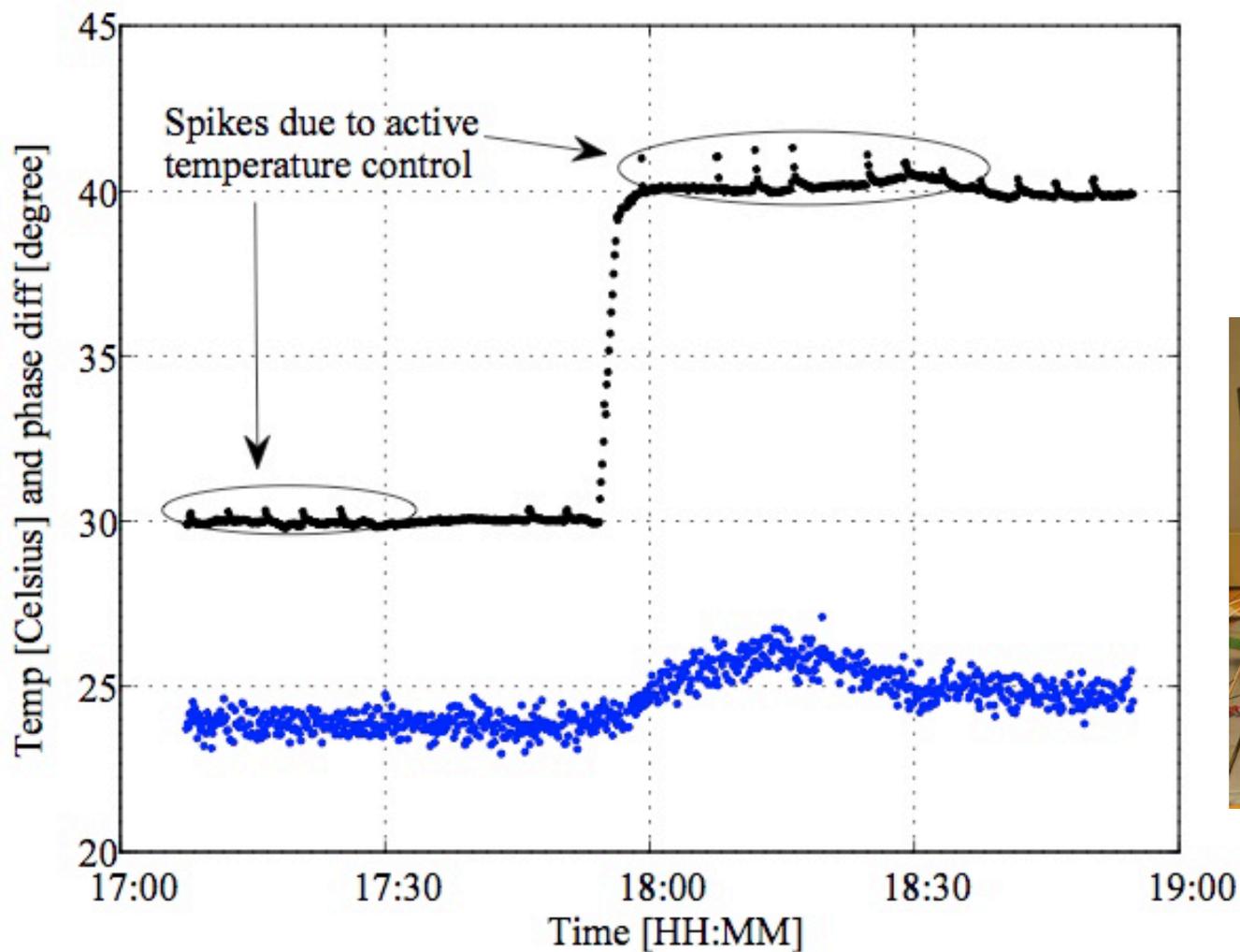
Thermal Analysis

- 35 GHz signals have a wavelength of 8.4 mm.
- Changes in the physical path length due to thermal expansion/contraction, will cause changes in the signal phase as will temperature imbalances in active components
- A one degree phase change is equivalent to 23 μm of electrical path length change. Integrated over 5 cm of total path length, this is equivalent to a 0.05% expansion coefficient, or 5 parts in 10,000.
- Thermal imbalances between the two interferometric paths will thus induce a temperature dependent phase error.
- We are measuring temperature “on-board” so that this phase error may be monitored and corrected in the digital stage.
- Point measures of temperature are unlikely to be sufficient to characterize the phase error, as they do not take into account temperature distributions or the thermal inertia of the chassis
- Thermal modeling will help understand the source of thermal imbalance as it is distributed throughout the system

Measurements of Differential Phase

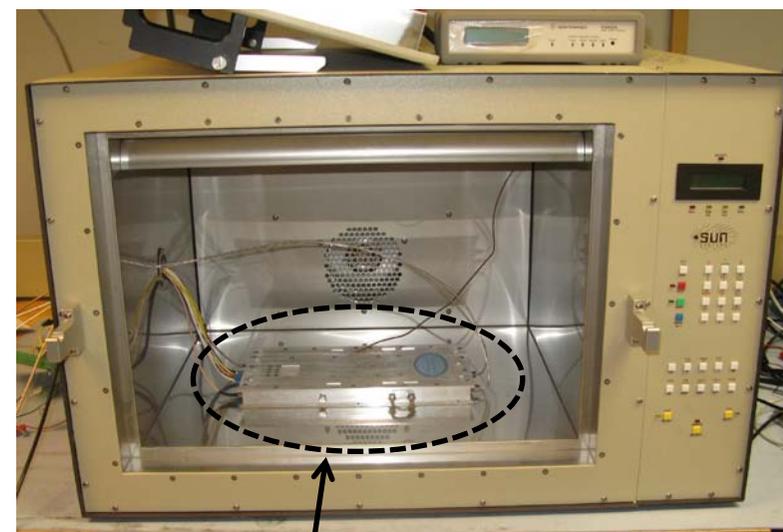


Thermal Testing and Characterization is a tricky affair



0.25°C/second, 15°C/min; -100°C to 300°C temperature range

Remote operation via serial port or IEEE-488 bus



downconverter

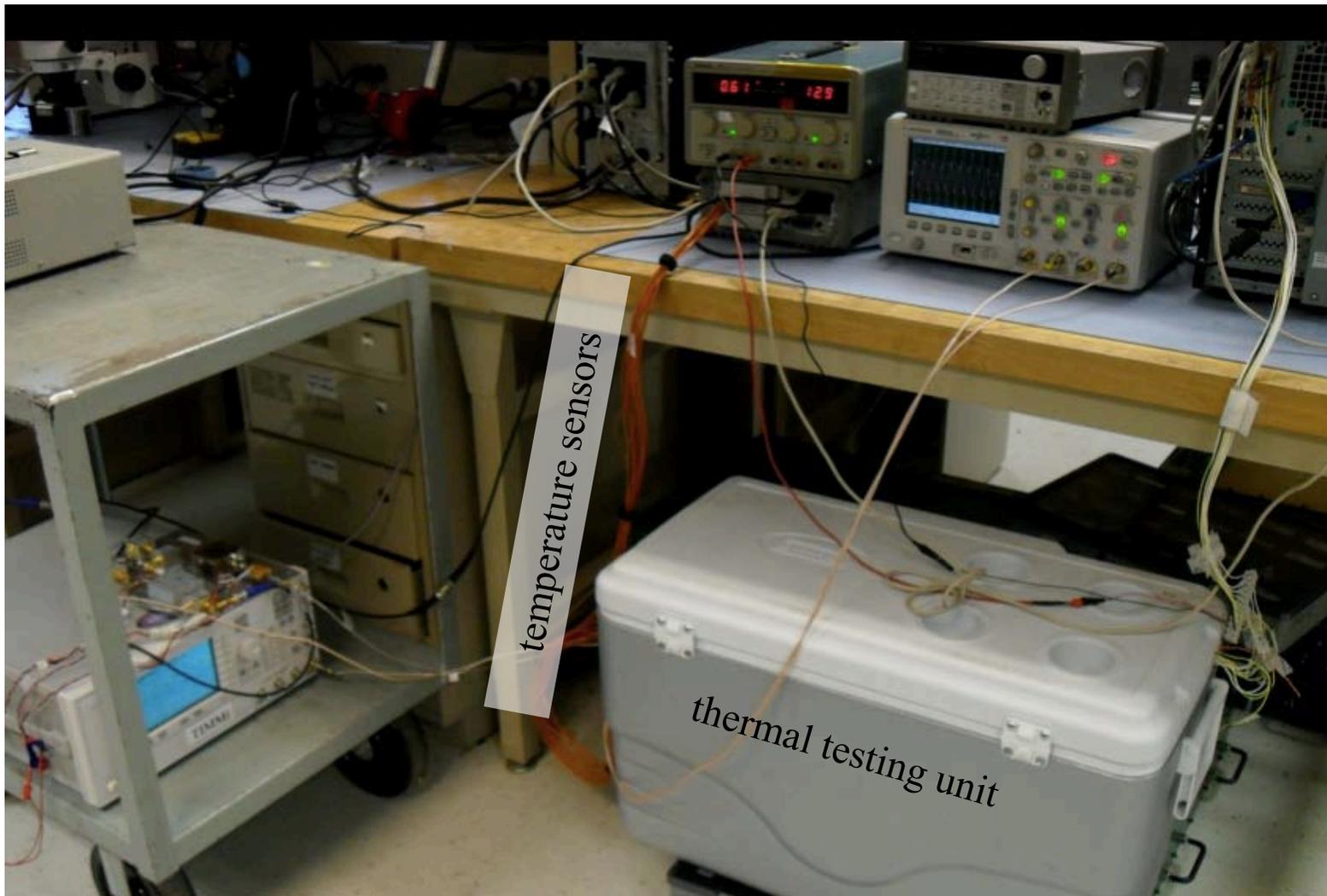
Active RF Testbed for the SWOT Mission

2011 ESTF

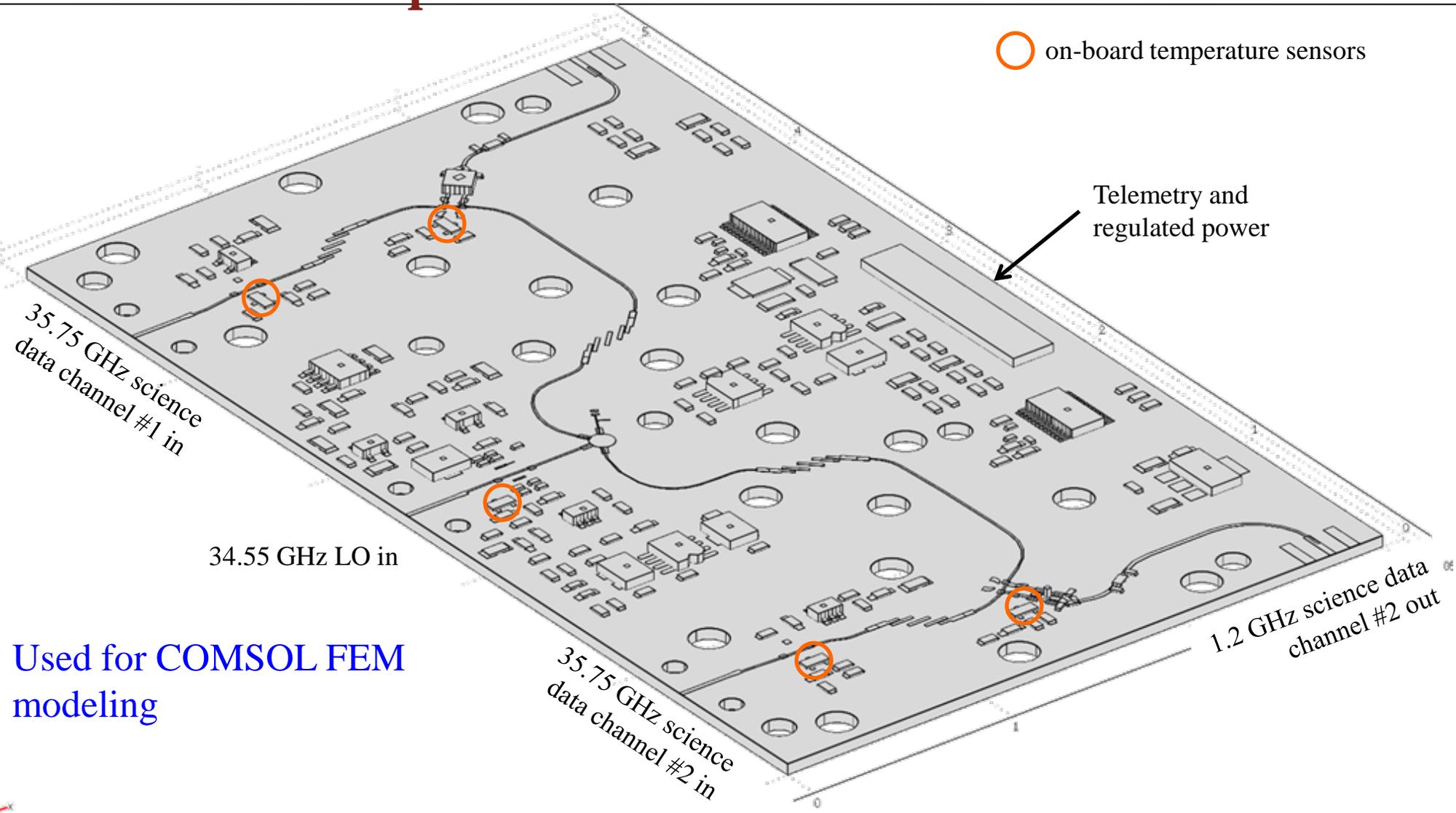
ESTO
Earth Science Technology Office



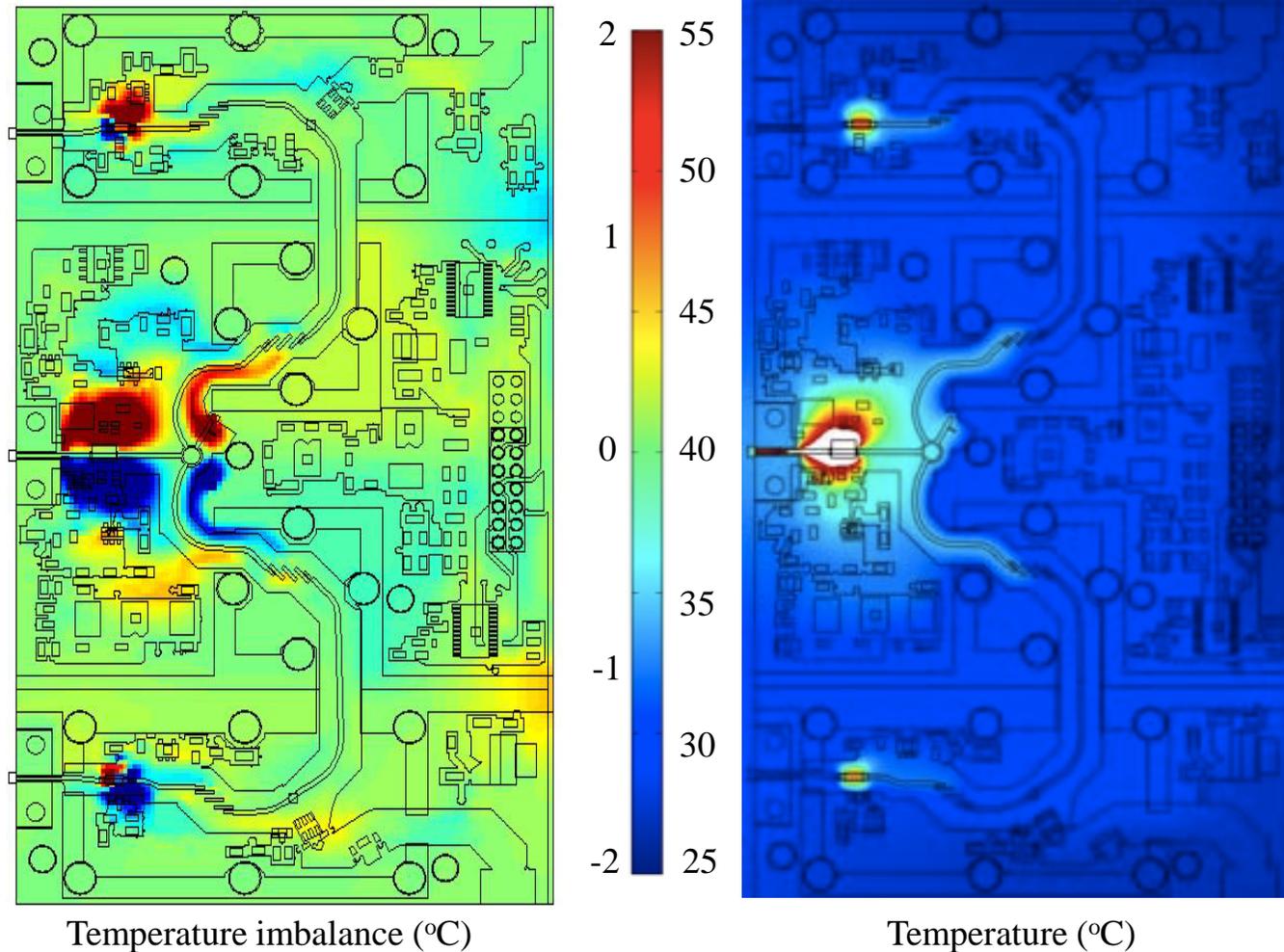
“Passive” thermal testing



A 3D-relief of previous Ka-band board

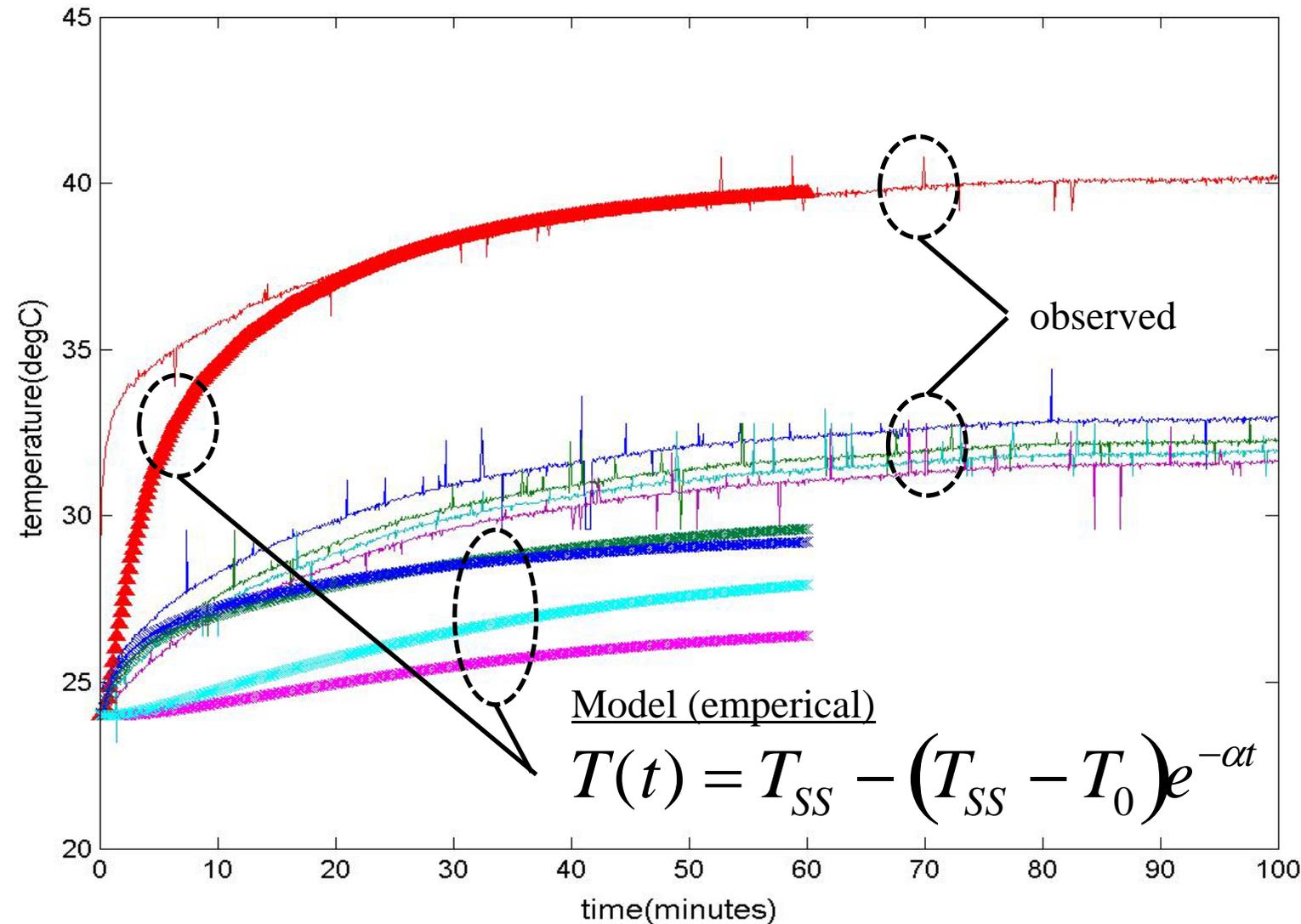


Modeled Thermal Imbalance



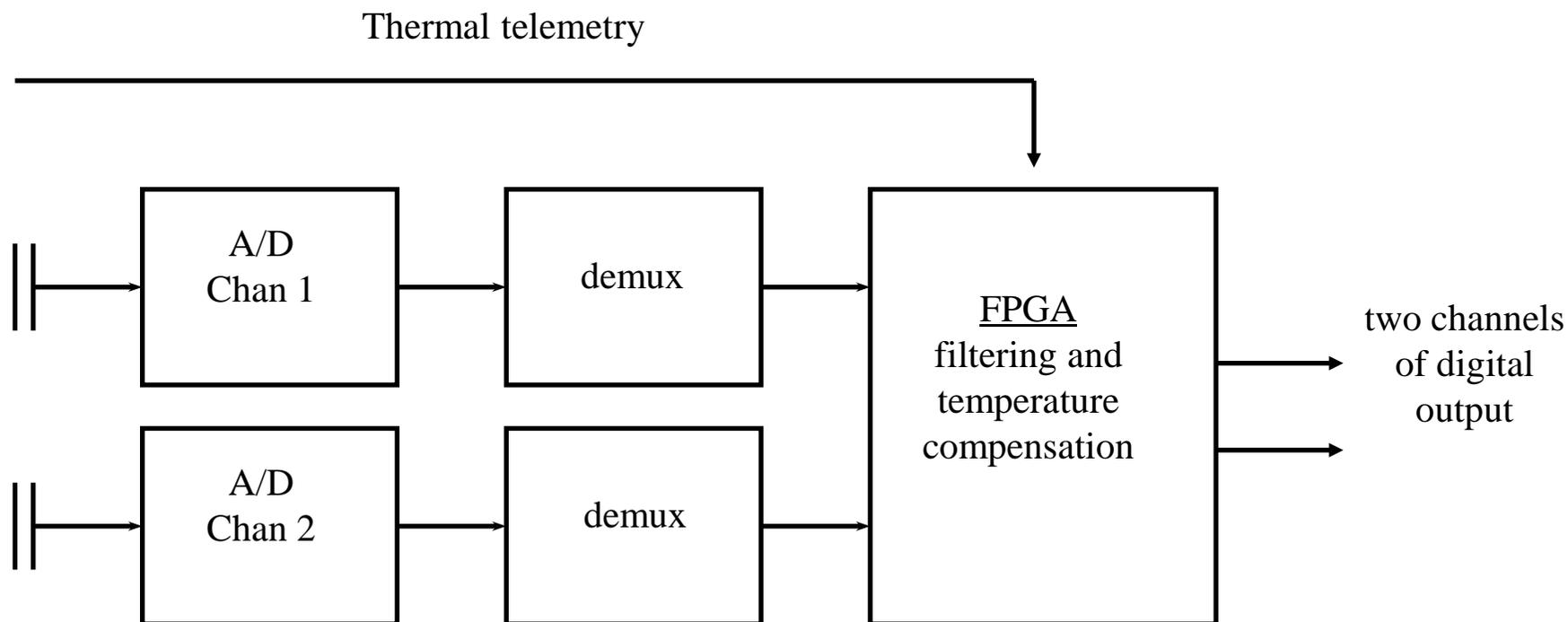
- COMSOL used to solve the heat equation and estimate board temperature and thermal imbalances.
- Thermal asymmetry in the downconverter design will lead to an asymmetry in the electrical path length.
- While this is not a bad thing in of itself, in a dynamic temperature environment, it will create a bias in the phase measurements, and hence the inferred height.

Dynamic Modeling of Temperature

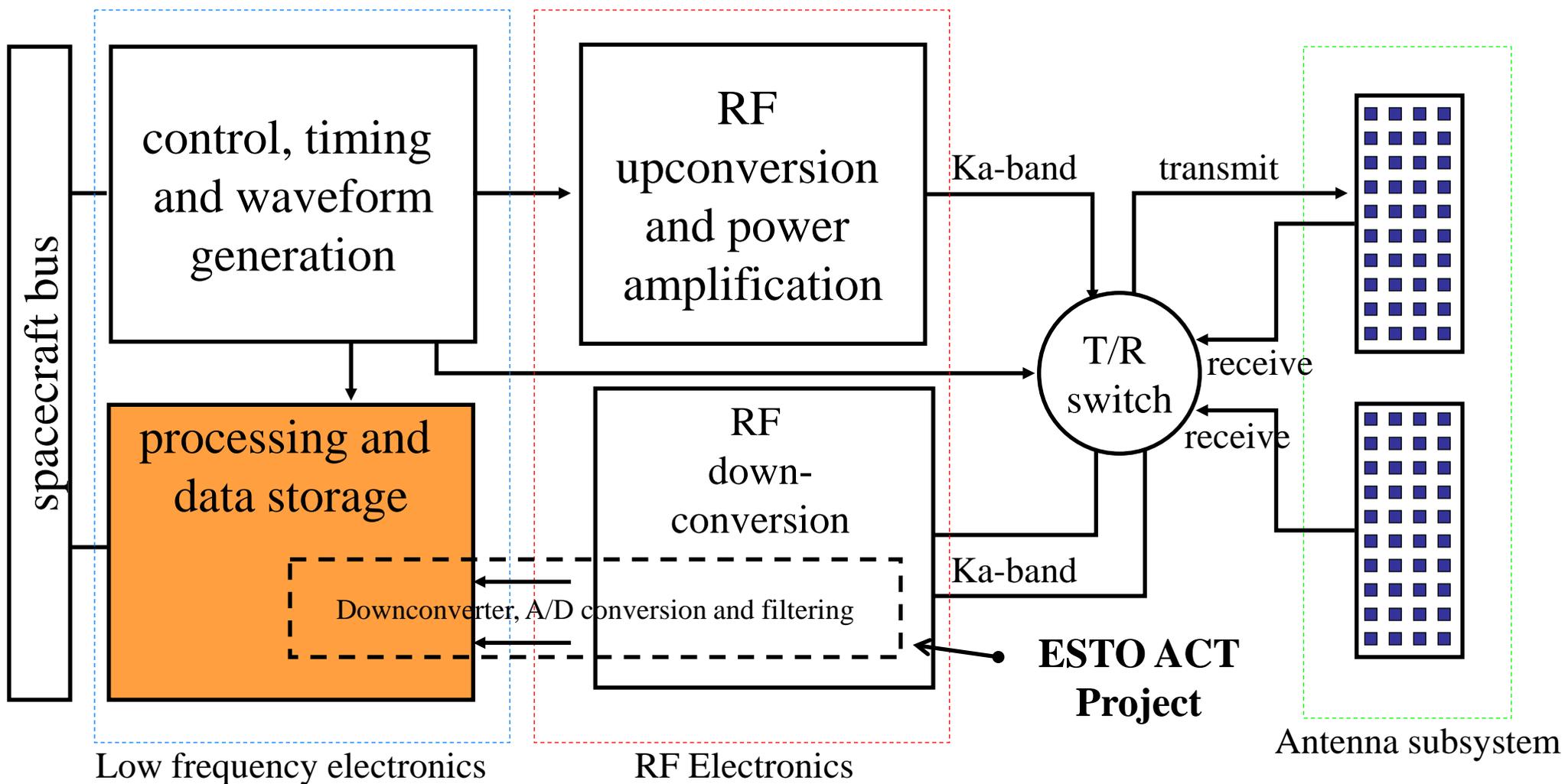


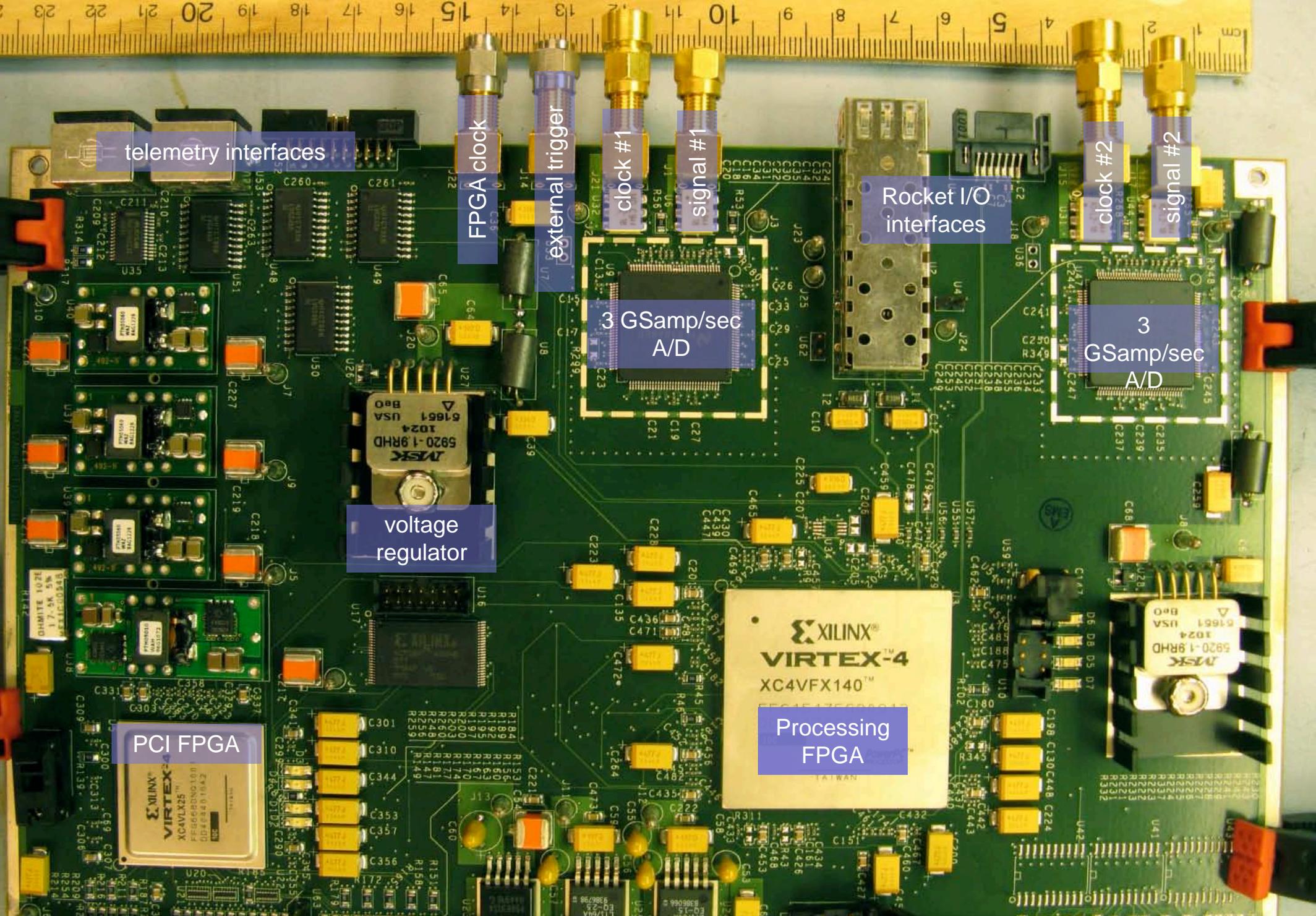
- Dynamic modeling of temperature is challenging because of the complexity of the subject matter
- Absolute accuracy is less important than the ability to capture the low order derivatives
- As modeling improves, we will incorporate the results into the observed phase behavior between the two channels
- Similar model results have been obtained using COMSOL. An emperical model is used currently for tuning the COMSOL model.
- Results will be used to better inform the microwave engineering

Thermal Telemetry combined with Science Data



Spacecraft block diagram





telemetry interfaces

FPGA clock

external trigger

clock #1

signal #1

Rocket I/O
interfaces

clock #2

signal #2

3 GSamp/sec
A/D

3
GSamp/sec
A/D

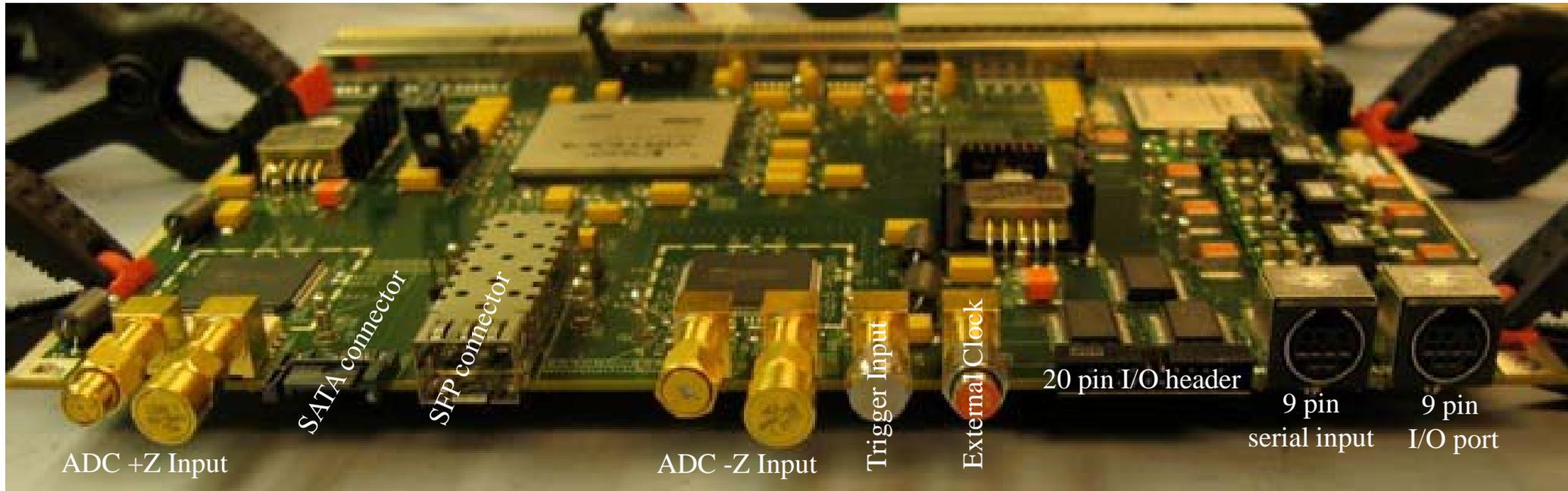
voltage
regulator

Processing
FPGA

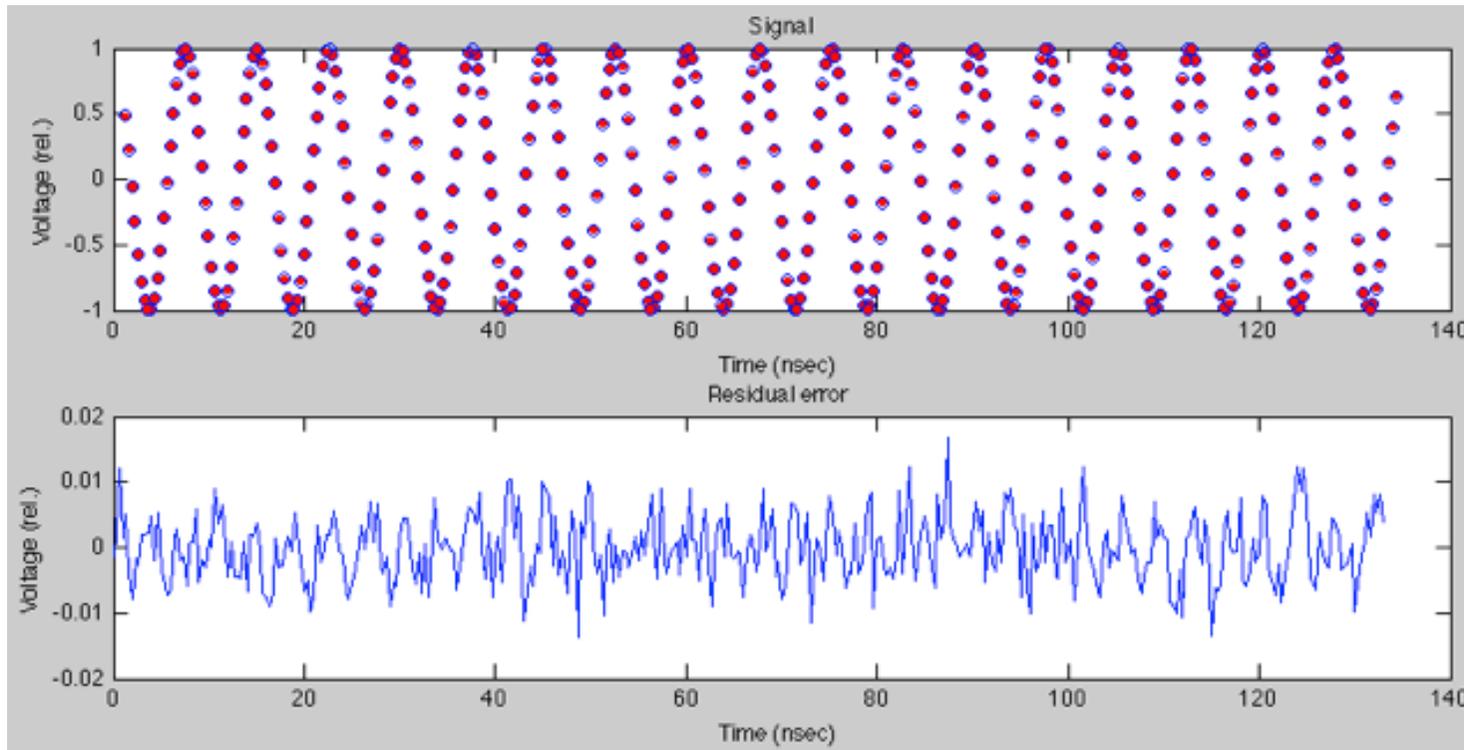
PCI FPGA

ESTO funded Analog to Digital & FPGA board using all space qualifiable parts

Front Panel Connections

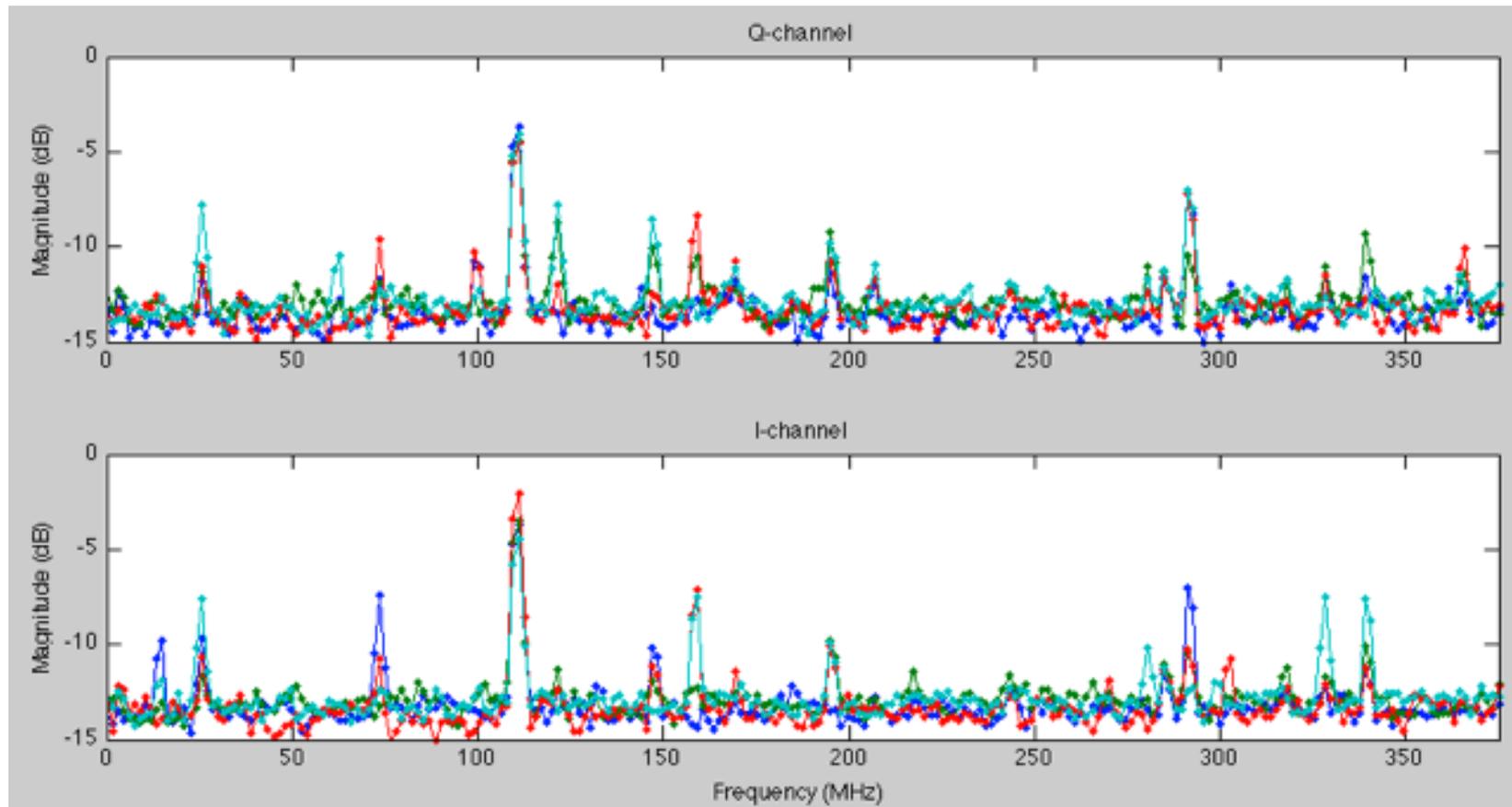


A/D performance validation



- Residual errors are less than $1/100^{\text{th}}$ of the input voltage (~ 40 dB in power)
- Dominated by quantization errors (7 bits ~ 44 dB QSNR)
- ENOB estimated to be 7 bits, close to the published ENOB of 7.2 bits

Error Spectra



- Error spectra used to determine periodic signals (e.g. clocks) which may be dominating the observed errors
- Dominant source at 110 MHz not yet identified, yet it is better than specification

FPGA and A/D board outreach

REAL TIME ESTIMATES OF DIFFERENTIAL SIGNAL PHASE FOR SPACEBORNE APPLICATIONS USING FPGAS

Vishwas Vijayendra, Paul Siqueira, Harikrishnan
Chandrikakutty, Akilesh Krishnamurthy, Russell Tessier

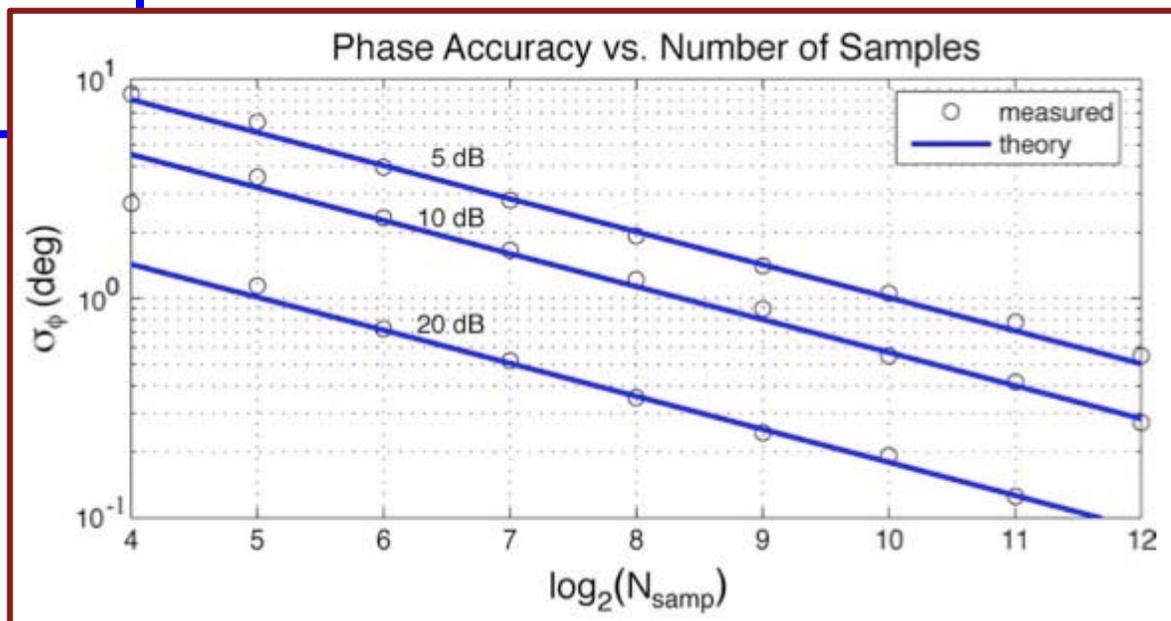
University of Massachusetts, Amherst

Funded by NASA ESTO GRANT #ACT-08-0048

- Basic form of algorithm
 - Feed a single tone signal into ADC and compare the resultant waveform with reference waveform
 - Differences are used to characterize phase and gain characteristics of the observed waveform



San Diego, June 5-9, 2011



Supporting Test Equipment



Arbitrary Waveform Generator (120 MHz BW); Agilent 1.25 GHz AWG also being used

40 GHz Spectrum Analyzer

40 GHz Signal Generator
TIMMi

2 GHz Signal Generator

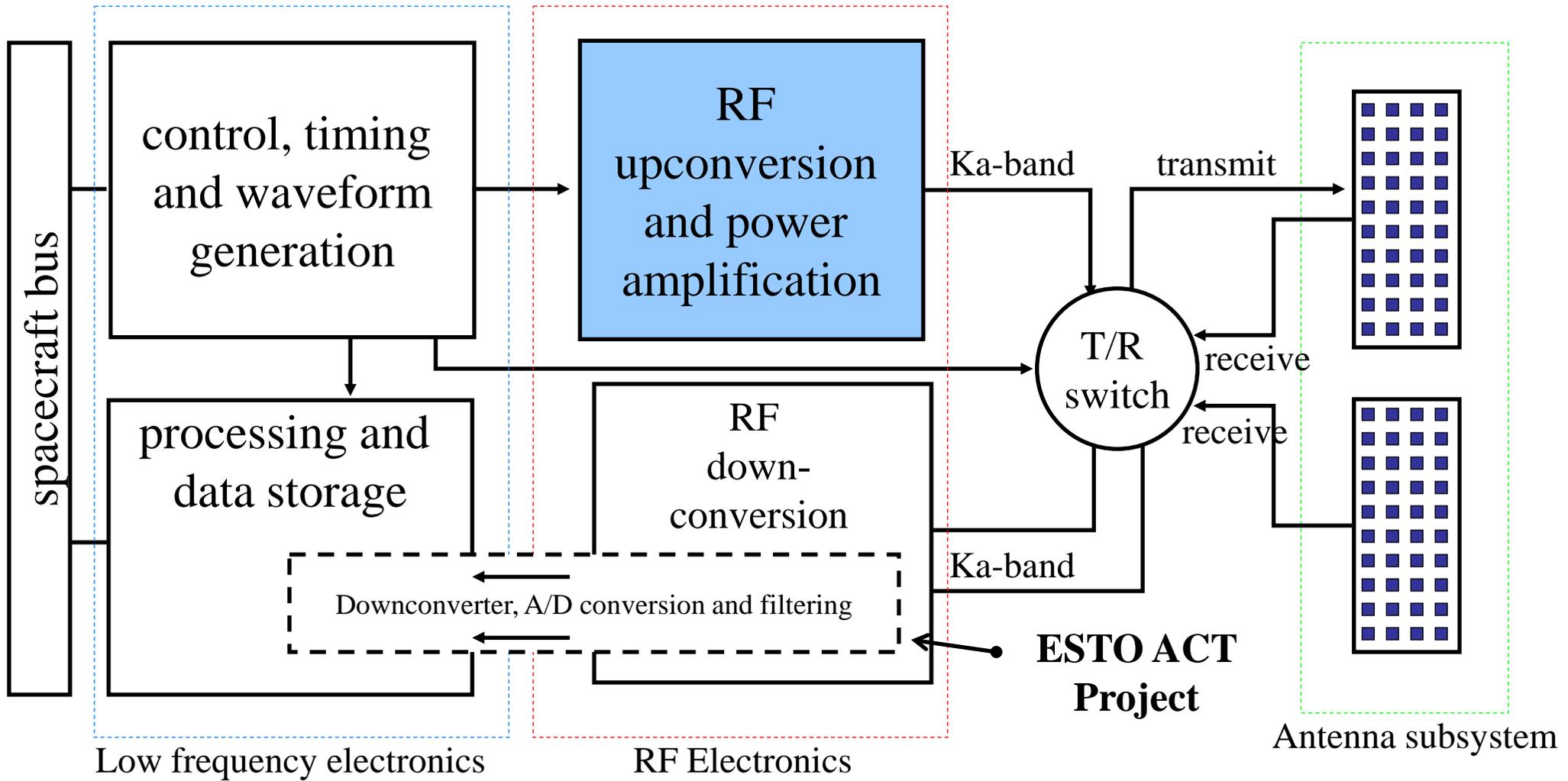
Digital Oscilloscope (1 GHz BW, 4 Gsamp/Sec)

Trigger Generator

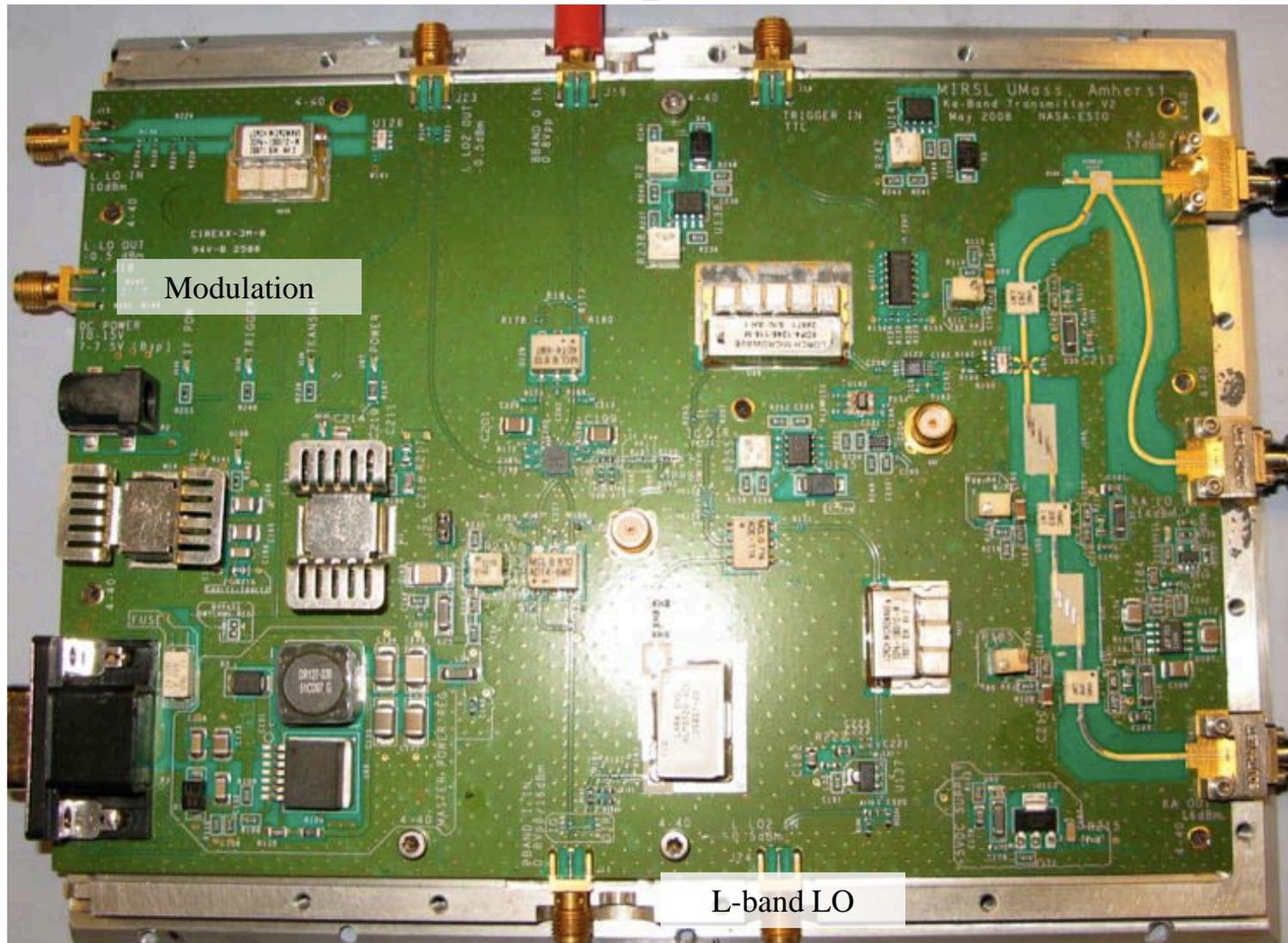
Power Supply

RF Electronics

Spacecraft block diagram



Baseband to Ka-band Upconverter



Ka-band LO out

Ka-band LO in

modulated Ka-band transmit signal

L-band LO

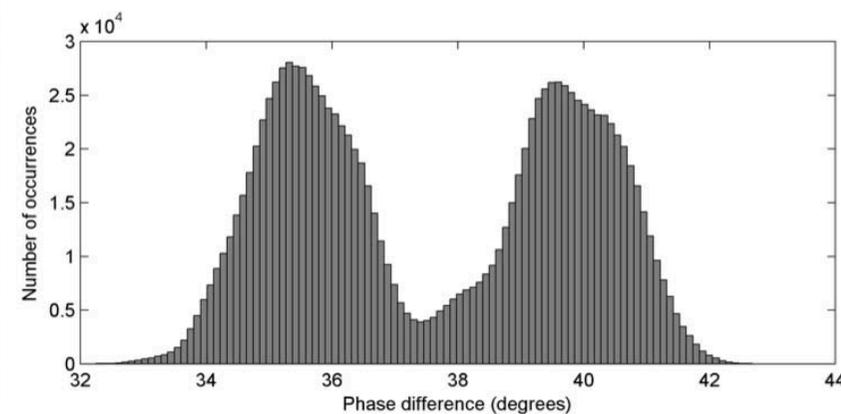
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Ka-band EIK (CPI) and HVPS (Pulse Systems)



- 1.5 kW 5% duty cycle extended interaction klystron (EIK) amplifier from CPI
- Modulator provided by Pulse Systems
- EIK Demand for large current from the HVPS at the PRF (4 kHz) causes an oscillation in the system phase performance



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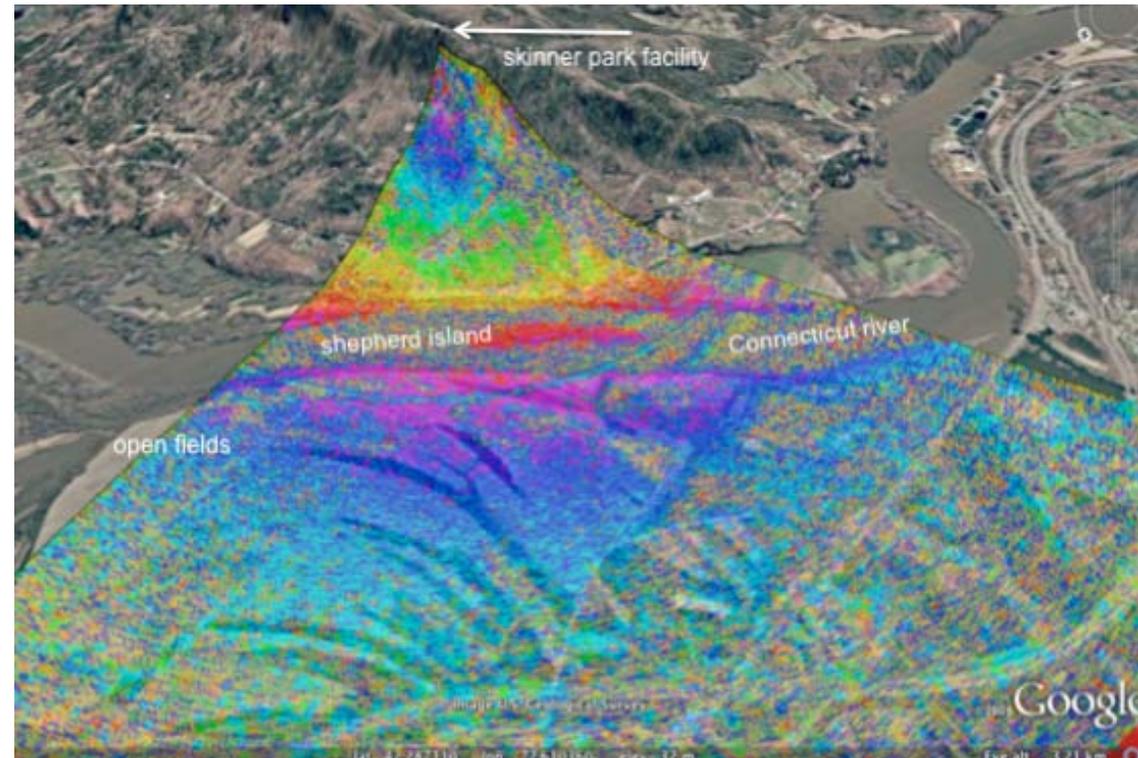
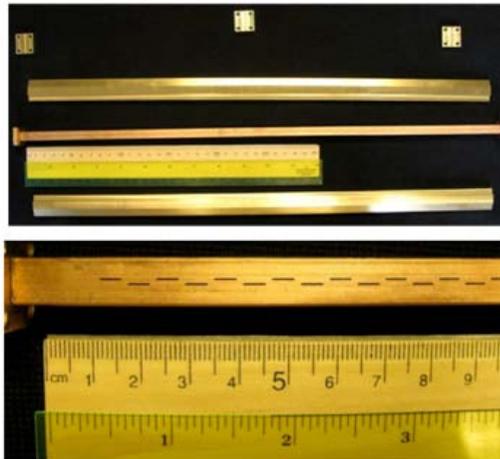
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Advancing the TRL

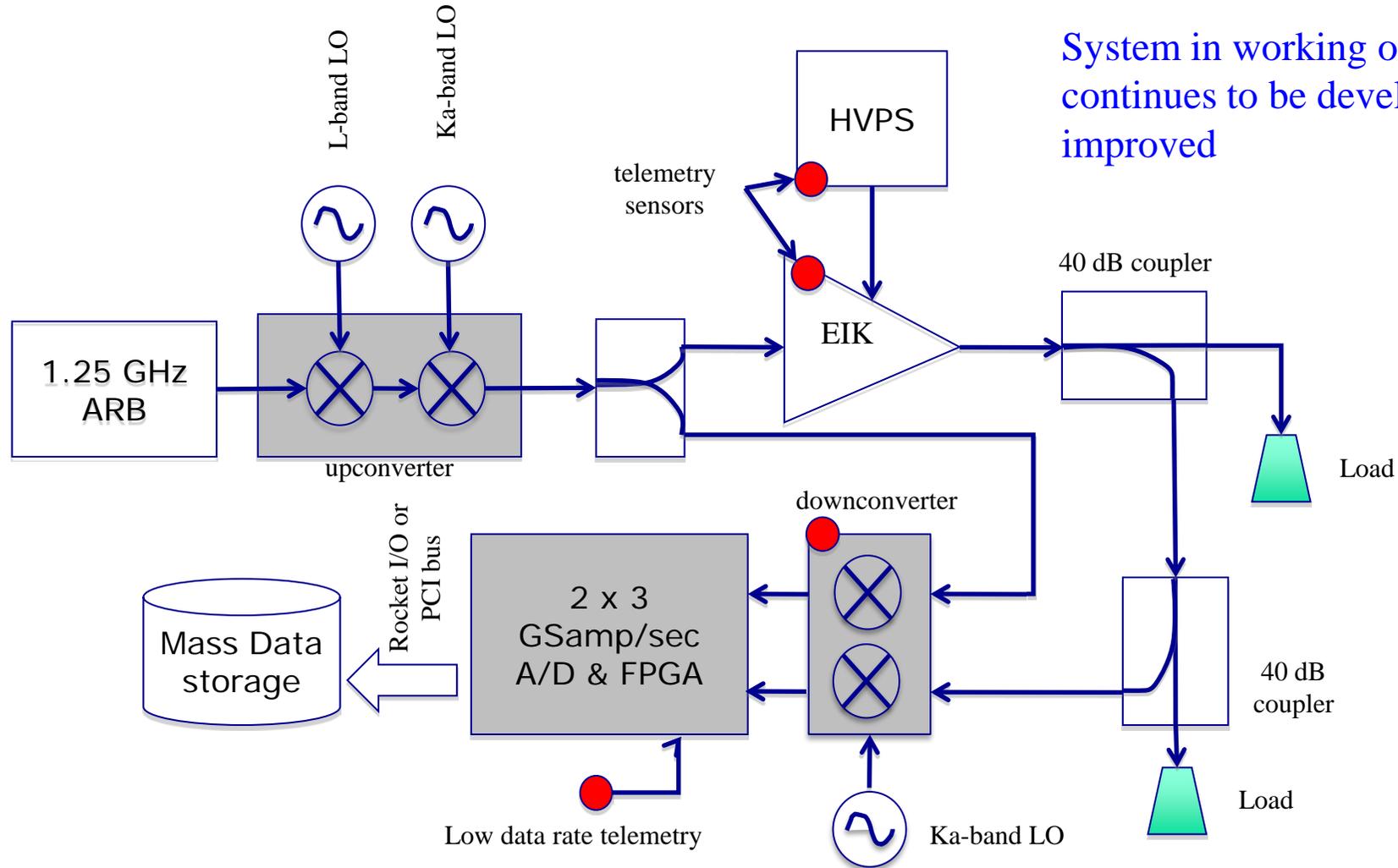


Working interferometer used for TRL advancement, integrated system testing and as a potential SWOT ground validation and pre-flight target characterization.



Active RF Testbed for the SWOT Mission

Block Diagram of RF Testbed



System in working order, continues to be developed and improved

- We are continuing our expertise in Ka-band microwave technology development
- Integration of RF hardware with digital subsystems allows detailed analysis of error in components and across the system
- Measurement acuity sufficient for measuring milligree variations in the propagation path
- Hardware components are valid across a variety of NASA mission types (e.g. GRACE II, SWOT)

Questions?